

MINE ENGINEERING SERVICES

Technical Report Update on the Copper, Gold, and Silver Resources and Pit Optimizations

MIRADOR PROJECT, ECUADOR



for

CORRIENTE RESOURCES INC.

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MINE DEVELOPMENT ASSOCIATES

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CONTENTS

1.0	SUMMARY		1
	1.1 Introduction		
	1.2 Geology and Mineralization		
	1.3 Sampling, Quality Assurance/Quality Co		
	1.4 Metallurgical Testwork		
	1.5 2005 Mineral Resource Estimate		
	1.6 2005 In-Pit Mineral Resources		
	1.7 Recommendations		
2.0	INTRODUCTION AND TERMS OF REFERE	NCE	10
	2.1 Introduction		10
	2.2 Terms of Reference		10
3.0	RELIANCE ON OTHER EXPERTS		12
4.0	PROPERTY DESCRIPTION AND LOCATION	V	13
	4.1 Property Location		13
	4.2 Mineral Tenure		13
	4.3 Permits and Agreements		20
	4.4 Environmental Impact Assessment		22
5.0	ACCESS ROUTES, CLIMATE, PHYSIOGRA	PHY AND INFRASTRUCTURE	23
	5.1 Access Routes		23
	5.2 Climate		23
	5.3 Physiography		23
	5.4 Infrastructure		23
6.0	HISTORY		25
	6.1 Exploration History		25
	6.2 2004 Mineral Resource Estimate (AMEC	C)	26
7.0	GEOLOGICAL SETTING		
	7.1 Regional Geology		29
	7.2 Local and Property Geology		29
8 N	DEPOSIT TYPES		33

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9.0	MINE	ERALIZATION	34
10.0	EXPI	ORATION	35
	10.1	2000	35
	10.2	2001	35
	10.3	2002	35
	10.4	2003	
	10.5	2004	
	10.6	2005	
11.0	DRIL	LING	37
12.0	SAM	PLING METHOD AND APPROACH	44
13.0	SAM	PLE PREPARATION, ANALYSES, AND SECURITY	16
13.0	13.1	Sample Preparation and Analyses 2000-2004	
	13.1	•	
		Sample Preparation and Analyses 2005	
	13.3	Sample Security	4/
14.0		A VERIFICATION	
	14.1	Introduction	
	14.2	Definitions	
	14.3	Quality Assurance/Quality Control (QA/QC) Programs 2000-2004	49
		14.3.1 ICP Sample Analysis	50
		14.3.2 Reassay of Phase 1 and 2 Drilling Samples	50
		14.3.3 Standard Reference Material	52
		14.3.4 Duplicate Samples	55
		14.3.5 Coarse Crush Duplicates, ½" Crush Material	55
		14.3.6 Coarse Reject Duplicates	
		14.3.7 Pulp Duplicates	
		14.3.8 Database Quality Control	
		14.3.9 Assay Results and Lithology Codes	
		14.3.10 Downhole Surveys	
		14.3.11 Bulk Density	
	14.4	Quality Assurance/Quality Control (QA/QC) Program 2005	
	14.4		
		14.4.1 Summary and Conclusions	
		14.4.2 Sample Preparation and Analysis	
		14.4.3 Duplicate Analyses on Pulps and Coarse Rejects	
150	4514	•	
15.0	ADJA	ACENT PROPERTIES	77
16.0		ERAL PROCESSING AND METALLURGICAL TESTING	
	16.1	Introduction	
	16.2	History of Metallurgical Testwork	
	16.3	Flowsheet	81



17.0	MINE	ERAL RESOURCE AND MINERAL RESERVE ESTIMATES	83
	17.1	Introduction	83
	17.2	Corriente Geologic Model	83
	17.3	Sample Coding and Compositing	86
	17.4	Specific Gravity Model	87
	17.5	Resource Model and Estimation	87
	17.6	Resource	
	17.7	Discussion, Qualifications, Risk and Recommendations	101
18.0	OTHI	ER RELEVANT DATA AND INFORMATION	103
	18.1	Introduction	103
	18.2	Floating Cone Analyses	103
	18.3	Production Schedules	105
	18.4	Economic Model	106
19.0		JIREMENTS FOR TECHNICAL REPORTS ON PRODUCTION AND DEVE	
	PROF	PERTIES	109
20.0	CON	CLUSIONS	111
21.0	RECO	OMMENDATIONS	113
22.0	REFE	RENCES	114
23.0	CERT	TIFICATE OF QUALIFIED PERSON	115
TAB	LES		
Table	1.1 Cri	teria for Resource Classification	5
		source Estimate Summary	
		asured and Indicated Resources Within Optimized Pit	
		ating Cone Parameters	
		rador Concession Locations and Areas	
		nual Conservation Patent Fees Payable For Mineral Concessions In Ecuador	
		t of Major Permits required for the Project	
		rador Deposit Mineral Resource Summary – 23 September 2004	
		etal Grades by Vertical vs. Angle Hole	
		ulk Density Independent Check Results	
		atistics of the Duplicate Samples	
		bsolute Value of the Relative Difference between Sample Pairs	
		st of Re-Analyzed Batches	
		escriptive Statistics of the Standard Reference Material	
		oding and Description of the Geologic Model	
		st of Specific Gravity Values Used in Model	
Table	17.3 E	stimation Parameters for Copper by Mineral Domain	91



Table 17.4 Estimation Parameters for Gold by Mineral Domain	93
Table 17.5 Estimation Parameters for Silver by Mineral Domain	94
Table 17.6 Criteria for Resource Classification	95
Table 17.7 Mirador Copper, Gold and Silver Resources – Measured	97
Table 17.8 Mirador Copper, Gold and Silver Resources – Indicated	97
Table 17.9 Mirador Copper, Gold and Silver Resources – Measured and Indicated	
Table 17.10 Mirador Copper, Gold and Silver Resources –Inferred	98
Table 17.11 Comparison of 2005 and 2004 (AMEC) Resource Estimates	99
Table 17.12 Comparison of 2005 and 2004 (AMEC) Resource Estimates – Inside AMEC Pit	100
Table 18.1 Floating Cone Parameters	
Table 18.2 Floating Cone Results	
Table 18.3 25,000 Tonnes per Day Production Schedule	
Table 18.4 50,000 Tonnes per Day Production Schedule	106
Table 18.5 Economic Model Inputs	
Table 18.6 Economic Model Results, 25,000 tpd Case (8% discount rate)	
Table 18.7 Economic Model Results, 50,000 tpd Case (8% discount rate)	
Table 18.8 25,000 tpd Case Initial Capital	108
FIGURES Figure 4.1 Location Map	14
Figure 4.2 Concession Location Map	
Figure 4.3 Detailed Map of the Mirador Concessions	
Figure 4.4 Detailed Map of the Mirador Property Rights	
Figure 7.1 Typical Cross Section (450) - Geology	
Figure 7.2 Drill Core Photo of DDH M64 Showing Low RQD	
Figure 7.3 Drill Core with Unaltered Anhydrite (Below the Gypsum Front)	
Figure 11.1 Mirador Drill Hole Location Plan	
Figure 11.2 Drill hole Collar Marker	
Figure 11.3 Core Recovery Statistics by Material Type	
Figure 11.4 RQD Recovery Statistics by Material Type	
Figure 12.1 Core Saw Facility	
Figure 14.1 QA/QC Reassay of Historical Data, Cu (ppm)	51
Figure 14.2 Reassay of Historical Data, Au (g/t)	
Figure 14.3 Percentile Rank Chart, Reassay Results, Cu (ppm), 501 Samples	52
Figure 14.4 Percentile Rank Chart, Reassay Results, Au (g/t), 442 Samples	
Figure 14.5 MS1 Round Robin and Sampling Results, Au (g/t), (DDH M63 to M90)	53
Figure 14.6 MS1 Round Robin and Sampling Results, Cu (%), (DDH M63 to M90)	
Figure 14.7 MS2 Round Robin and Sampling Results, Au (g/t), (DDH M72 to M90)	
Figure 14.8 MS2 Round Robin and Sampling Results, Cu (%), (DDH M72 to M90)	
Figure 14.9 Coarse Crush Duplicate Results, Cu %, 27 Data Pairs	
Figure 14.10 Coarse Crush Duplicate Results, Au g/t, 27 Data Pairs	
Figure 14.11 Coarse Reject Duplicate Results, Cu %, Scatter Plot	
Figure 14.12 Coarse Reject Duplicate Results, Au g/t, Scatter Plot	58

Figure 14.13 Duplicate Results, Cu %, Percentile Rank Chart	58
Figure 14.14 Duplicate Results, Au g/t, Percentile Rank Chart	59
Figure 14.15 Pulp Duplicate Results, Cu %, Scatter Plot	60
Figure 14.16 Pulp Duplicate Results, Au g/t, Scatter Plot	60
Figure 14.17 Copper Duplicate Assays – Pulps	65
Figure 14.18 Gold Duplicate Assays – Pulps	65
Figure 14.19 Copper Duplicate Assays – Coarse Rejects	66
Figure 14.20 Gold Duplicate Assays – Coarse Rejects	66
Figure 14.21 Relative Differences of Copper Duplicate Assays – Pulps	69
Figure 14.22 Relative Differences of Gold Duplicate Assays – Pulps	69
Figure 14.23 Relative Differences of Copper Duplicate Assays – Coarse Rejects	70
Figure 14.24 Relative Differences of Gold Duplicate Assays – Coarse Rejects	70
Figure 14.25 Absolute Value of the Relative Difference of Copper Duplicate Assays – Pulps	71
Figure 14.26 Absolute Value of the Relative Difference of Gold Duplicate Assays – Pulps	71
Figure 14.27 Absolute Value of the Relative Difference of Copper Duplicate Assays –Coarse Re	jects.72
Figure 14.28 Absolute Value of the Relative Difference of Gold Duplicate Assays -Coarse Rejection	cts72
Figure 14.29 Standard MS1 Checks – Copper	74
Figure 14.30 Standard MS1 Checks – Gold	
Figure 14.31 Standard MS2 Checks – Copper	
Figure 14.32 Standard MS2 Checks – Gold	75
Figure 16.1 Simplified Mirador Flowsheet	82
Figure 17.1 Schematic Illustration of Rock and Mineral Zones Used for Estimation - Copper	85
Figure 17.2 Schematic Illustration of Rock and Mineral Zones Used for Estimation –Gold and St	ilver85
Figure 17.3 Typical Cross Section (450) with Block Grades – Copper	89
Figure 17.4 Typical Cross Section (450) with Block Grades - Gold	90
Figure 17.5 Typical Cross Section (450) with Block Classification	96

APPENDICES

Appendix A Report of P&T Asesores Legales, Abogados, including Map and Tables

Appendix B Mirador Drill Holes M-1 to M-141 Locations, Orientations and Lengths

Appendix C Sample Descriptive Statistics for Copper, Gold, and Silver



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1.0 SUMMARY

1.1 Introduction

Corriente Resources Inc. ("Corriente") engaged Mine Development Associates ("MDA") to provide an updated mineral resource estimate and a Technical Report for its Mirador Project in southeastern Ecuador. Steven Ristorcelli, Principal Geologist for MDA, served as the Qualified Person responsible for preparing the mineral resource estimation. This Technical Report was prepared by Steven Ristorcelli P.Geo., Scott Hardy P.Eng. of MDA, George Sivertz, P.Geo., Senior Geologist, OreQuest Consultants Ltd. and John Hoffert P.Eng. of Hoffert Processing Solutions Inc. This report provides a summary of Mirador Project work conducted since 2000, and an update and review of the Mirador Project activities that took place in 2005.

The last National Instrument ("NI") 43-101-compliant Technical Report for the Mirador project was filed by AMEC Americas Limited ("AMEC") in October 2004. Since that time, Corriente has advanced the Mirador project through a number of important new studies and work programs:

- A Feasibility Study Report, completed in May 2005 (AMEC Americas Limited filed on SEDAR on May 13, 2005);
- A 52-hole, 11,935-m core-drilling program;
- An updated copper, gold, and silver resource estimate, and pit optimizations on the Mirador resource; and
- The filing of an Environmental Impact Assessment ("EIA") Report with supporting documentation, in December 2005.

The Mirador property comprises six contiguous mineral concessions that cover an area of 13,640 hectares (13.64 sq²). The Mirador concessions are centered 10 km east of the Rio Zamora (Zamora River) in the Zamora-Chinchipe Province of southeastern Ecuador. The eastern property boundary is adjacent to the Ecuador-Perú border. The concessions are approximately 340 km south of Ecuador's capital city of Quito and 70 km east-southeast of the city of Cuenca.

BHP Billiton S.A. ("Billiton") began regional exploration in southeastern Ecuador in 1994 and identified a number of possible porphyry copper targets in the region. In April 2000, Billiton and Corriente entered into an agreement covering 230 sq km of mineral concessions in the southern part of the region, including the area of the Mirador property.

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Corriente has carried out exploration on the Mirador property since April 2000. The work completed included geological mapping, geochemical soil sampling, rock chip sampling, and the completion of 36,284 m of core drilling in 143 diamond drill holes. Corriente, through its wholly-owned subsidiary companies in Ecuador, holds a 100% interest in the Mirador property. Billiton holds a 2% Net Smelter Royalty interest in the Mirador deposit.

In November 2003, Corriente commissioned AMEC to be the primary consultant for the preparation of a bankable feasibility study for the Mirador project. Knight Piésold Ltd was responsible for the design of a tailings management facility and related infrastructure, and Merit Consultants International Inc. provided study coordination, project planning/scheduling, and capital cost estimates. The Feasibility Study Report was completed in May 2005. Corriente engaged AMEC in 2004 to provide a mineral resource estimate and Technical Report for the Mirador project.

In 2005, Corriente completed 11,935 m of core drilling in 52 holes. This program was in large part aimed at better defining the distribution of weakly-mineralized porphyry dikes and breccias, which account for most of the lower-grade zones in the deposit. Another benefit was improved resolution of the distribution of higher-grade supergene copper mineralization. The geological data from the drill holes, together with new information from outcrops exposed during the construction of new drill trails, helped to confirm and refine contacts of the porphyry dikes, particularly in the northern sector. A few holes targeted the breccia dikes in the north part of the deposit, to better locate and define their contacts and to explore for potentially economic copper mineralization along their margins. The 2005 holes did not intersect any sizeable new dikes, or locate any important new areas of mineralization, so little revision of the geological model was required.

In the fourth quarter of 2005, Corriente retained MDA to prepare an updated mineral resource estimate and to conduct pit optimization studies. The purpose of the mineral resource estimate update was to incorporate the new data from the fifty-two drill holes completed in 2005 into the resource model. MDA relied upon certain results of previously published work, and used procedures similar to those used by AMEC in the preparation of the 2004 mineral resource estimate. MDA reported Measured and Indicated Mineral Resources of 437,670,000 tonnes grading 0.61% Cu, 190 parts per billion (ppb) gold, and 1.5 parts per million (ppm) silver, at a 0.40% Cu cutoff grade. Inferred Mineral Resources, also at a 0.40% Cu cutoff, were stated as 235,400,000 tonnes grading 0.52% Cu, 170 ppb gold, and 1.3 ppm silver. The MDA estimate places more material in the Measured and Indicated resource category than was reported by AMEC in 2004, at a slightly lower grade. These changes are the direct result of the inclusion of new data from the 2005 infill drilling program.

1.2 Geology and Mineralization

The copper-gold-silver mineralization of the Mirador deposit is hosted by a Late Jurassic porphyry intrusive phase of the Zamora Batholith. The northern section of the Mirador deposit subcrops under leached rock, weathered rubble and overburden; the southern extremity is overlain by Cretaceous quartz sandstone.



The Zamora batholith forms the wall rocks of the Mirador porphyry copper-gold system. Within the mineralized zone, the intrusion consists mainly of equigranular Zamora granite and granodiorite. In drill core, the Zamora granite appears highly fractured; this is a weathering effect due to the dissolution of anhydrite and gypsum from veinlets. Where anhydrite is unaltered by weathering and leaching, the drill core is relatively competent.

Near the center of the mineralized system is a large body of breccia, interpreted to be an intrusive pipe or diatreme. This mineralized breccia is composed of angular fragments of porphyry dikes, Zamora granite, and quartz-vein fragments. Northeast-striking, northwest-dipping hornblende-feldspar porphyry dikes cut the breccia and the wall rocks of the deposit. Weakly developed zones of supergene copper (and possibly silver) enrichment lie beneath a leached "cap" that averages less than 22-m thick.

The sequence of mineral deposition at Mirador has been divided into early-stage molybdenum, early-stage copper \pm gold, and late-stage copper-gold events, with a final weak polymetallic vein stage. Both copper-gold depositional events are dominated by chalcopyrite, with traces of native gold. Molybdenite is present in systems of early-stage quartz veins that have a preferred east-west orientation. These veins occur as stockwork in both Zamora granite and early porphyry dikes.

1.3 Sampling, Quality Assurance/Quality Control and Check Sampling

In all the drilling campaigns, Corriente used consistent strategies for sampling, sample preparation, and sample analysis. Split drill core samples were sent to preparation facilities in Ecuador, and 100-gram pulp sub-samples were shipped to analytical laboratories in Vancouver, Canada. Copper was analyzed by atomic absorption spectroscopy ("AAS") methods, and gold was determined by fire assay with an AAS finish. The names of the laboratories used and the details of sample preparation and analysis are provided in the pertinent sections of this report.

The quality assurance/quality control ("QA/QC") procedures used by Corriente became more sophisticated with successive drill campaigns. The early exploratory drill programs (2000-2002) did not incorporate fully adequate QA/QC procedures. To compensate for this, 5% of the sample pulps from these drill programs were sent to ALS Chemex in Vancouver, Canada in 2004 for re-analysis. The copper and gold grades from the re-analyzed check samples compared well to the grades from the original samples. Consequently, all of the original sample assays were considered to be sufficiently accurate to be used for mineral resource estimation purposes.

A more comprehensive QA/QC program was adopted by Corriente in 2004, following procedures recommended by AMEC. AMEC reviewed the duplicate sample analyses and concluded that the analytical results for copper indicated that the drill core sampling, sample preparation, and analytical procedures in use would lead to good quality copper analytical results for all samples. However, AMEC also noted that the gold data for the Mirador pulp duplicate samples indicated that, for 90% of the samples, there is an average difference of 15% between the gold grades of the pulp duplicate samples and the grades of the original pulp samples. AMEC concluded that this reflected a relatively low level



of precision and suggested that the causes of the effect were probably the relatively small weight of the sample shipped to the assay laboratory (100 grams), and the small fire assay aliquot weight (30 grams).

AMEC completed a data quality check on 5% of the sample database used for the 2004 resource estimation. The data were found to be of excellent quality and adequate for AMEC's resource estimation purposes.

The 2005 phase five drilling program involved the drilling of 11,935 m in 52 core holes (M91 to M141). Because of this drilling, the drill hole assay database now contains 3,592 additional assayed drill intercepts. MDA reviewed the results of the 2005 drilling program but did not take independent check samples from the 2005 drill holes. MDA did take independent samples from prior drilling campaigns.

For the 2005 drilling program, Corriente generally followed the QA/QC guidelines recommended by AMEC.

The sample preparation procedures are appropriate and well done, and the assays and analyses are of good quality. Based on the results of the analyses of standard samples inserted into the sample stream, there does not appear to be any significant bias in the analytical data. The results from the inserted blank samples indicate that the sample preparation procedures are conducted with appropriate care. Copper analyses of pulp duplicates reproduce well, while gold fire assays of pulp duplicates show modest variability. Although MDA does not believe that the modest variability in the reproducibility of gold assays has instilled any material bias or skewed the results, it is suggested that this be investigated with a set of metallic screen sample assays.

1.4 Metallurgical Testwork

The following is quoted *verbatim* from AMEC (2004).

A significant amount of metallurgical testwork has been undertaken on mineralized samples from the Mirador porphyry copper-gold porphyry deposit since 2002. SGS Lakefield Research (Lakefield), in Lakefield, Ontario carried out the main program of feasibility testing between December 2003 and September 2004. This included flowsheet development and mineralogical and recovery variability mapping programs on a total of about 3,000 kg of split diamond drill core from twenty drill holes and at various depths across the deposit. Overall this represents a reasonable spatial distribution of the expected metallurgy across the deposit.

The mill flow sheet selected for Mirador will be a conventional copper-gold porphyry flowsheet, with relatively coarse primary SAG and ball mill grinding to about 150 µm followed by copper rougher flotation, concentrate regrind to 25 µm, and cleaner flotation and dewatering. The process will be designed to treat 25,000 t/d. Concentrates produced are predicted to average 30% copper at a recovery of 91%. Gold recovery is expected to average 47%. A laboratory analysis of concentrates indicated that no significant deleterious penalty element impurities were present.



1.5 2005 Mineral Resource Estimate

Corriente requested that MDA complete a resource update on the Mirador Project. The motivation for the update was the inclusion of the 52 new drill holes that were completed in 2005. MDA relied on previous work and used procedures similar to those used by AMEC in the original work in 2004; unless evidence existed suggesting that new procedures should be used. The final results conform to CIM standards.

Resource estimation utilized a combination of mineral and lithologic domains defined in wireframe solids that were constructed by Corriente. Gold, silver, and copper generally occur together, and so are modeled in a similar manner except in the enriched, mixed, and leached zones, where gold and silver were modeled similarly but distinctly from copper. Specific gravity values used were similar to those used in previous modeling efforts, except that there were additional specific gravity data, and a 2% reduction factor was applied to account for sample-selection bias.

MDA estimated the resource using inverse distance to the fourth power, with a maximum of 14 samples per block and a maximum of four samples per hole. Search ranges varied depending upon the zone or lithology being estimated and reached 200 m. Resource classification criteria are presented in Table 1.1. A summary of the resources is presented in Table 1.2.

All – Measured

Minimum no. of samples /minimum no. of holes / maximum distance (m)

Hypogene – Indicated

Minimum no. of samples /minimum no. of holes / maximum distance (m)

Or

Minimum no. of samples /minimum no. of holes / maximum distance (m)

2 / 2 / 100

Or

Minimum no. of samples /minimum no. of holes / maximum distance (m)

2 / 1 / 35

Enriched (supergene) and Mixed – Indicated

Minimum no. of samples /minimum no. of holes / maximum distance (m)

Or

Minimum no. of samples /minimum no. of holes / maximum distance (m)

2 / 1 / 35

All material not classified above is Inferred

Table 1.1 Criteria for Resource Classification

MDA has reported resources to the 750-m elevation but has modeled down to elevations of 650 m. It is important to note that the deepest drill hole samples are from elevations of approximately 850 m and are mineralized. Pit optimization shells bottom out at 650 m (the bottom of the estimated model) when considering the Inferred material 200 m below the deepest drill intercept in the pit optimization and using "reasonable but optimistic" pit optimization parameters.

Leached – modeled but unclassified; all Leached material is considered to be waste



Table 1.2 Resource Estimate Summary

leasured	

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	52,610,000	0.65	753,000,000	210	360,000	1.6	2,770,000

Total Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	385,060,000	0.60	5,134,000,000	190	2,380,000	1.5	18,760,000

Total Measured and Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	437,670,000	0.61	5,887,000,000	190	2,740,000	1.5	21,530,000

Total Inferred

I	Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
	0.40	235,400,000	0.52	2,708,000,000	170	1,250,000	1.3	9,900,000

Hypogene Measured

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	50,880,000	0.64	717,640,000	210	340,000	1.6	2,650,000

Hypogene Indicated

, 60 90							
Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	375,150,000	0.60	4,954,310,000	190	2,310,000	1.5	18,130,000

Hypogene Measured and Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	426,030,000	0.60	5,671,950,000	190	2,650,000	1.5	20,780,000

Hypogene Inferred

117 1 3 2 1 1 1							
Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	233,240,000	0.52	2,680,480,000	170	1,240,000	1.3	9,850,000

Supergene* Measured

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	1,710,000	0.94	35,280,000	220	12,000	2.0	112,000

Supergene* Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	9,650,000	0.83	176,190,000	210	60,000	2.0	610,000

Supergene* Measured and Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	11,360,000	0.84	211,470,000	200	72,000	2.0	722,000

Supergene* Inferred

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	1,033,000	0.67	15,185,000	170	5,600	1.3	44,000

^{*} Supergene includes mixed and enriched; no leached material is tabulated in Measured, Indicated or Inferred

*total Measured plus Indicated resources were calculated from rounded Measured and rounded Indicated resources and hence some apparent differences are rounding related.



1.6 2005 In-Pit Mineral Resources

In-pit mineral resources for the Mirador project were developed by applying relevant economic and engineering criteria to MDA's estimated Measured and Indicated resources in order to define the economically extractable portions (Table 1.3). MDA based the Mirador in-pit mineral resources on the AMEC 2005 feasibility study that MDA believes to be reasonably accurate and current. The significant change from the feasibility is an increase in pit size, which is a result of not limiting the mine life. Operating costs are based on mining and processing 25,000 tonnes of mill feed per day and mining costs may change if the planned production rates change.

Table 1.3 Measured and Indicated Resources Within Optimized Pit

Class	Tonnes	Cu %	Au	Ag	Waste Tonnes	Total Tonnes	Strip
	(000)		(ppb)	(g/t)	(000)	(000)	ratio
Total	346,995	0.62	196	1.57	491,393	838,388	1.4

MDA used the Medsystem© Lerchs-Grossmann "floating cone" algorithm to produce open-pit cone shells using the parameters shown in Table 1.4. Only Measured and Indicated materials were allowed to make a positive economic contribution; Inferred material is considered waste. The cutoff grade for the base case (\$1.00/lb Cu price), assuming only copper revenue, is 0.37% Cu. Because recovered gold contributes value, the actual cutoff is slightly lower depending on the gold grade.

MDA designed an ultimate pit using the base-case floating cone (Cu \$1.00/lb, Au \$400/oz) as a template. Haul roads were designed with a maximum 10% grade and a width of 22 m. This should accommodate haul trucks of 90-tonne capacity, which are about 7-m wide.

AMEC reported preliminary pit slope angles and designs in the 2005 feasibility. These slopes, adjusted for inclusion of ramps were used in the floating cone runs. Corriente engaged Piteau Associates ("Piteau") to continue with the geotechnical work and recommend final pit slopes, a work that is still in process at the time of this writing. Piteau provided preliminary slope-angle ranges and design sectors, the more conservative of which were used in these pit designs. The conservative Piteau angles are similar to the AMEC slopes. The pit design could change if the slope criteria change in the final Piteau work.



Table 1.4 Floating Cone Parameters

Item	Va	ılue
Copper Processing		
Mill recovery %		91.4%
Concentrate grade %		30%
Concentrate moisture %		8%
Concentrate losses %		0.25%
Concentrate transport \$/WMT	\$	81.62
Concentrate transport \$/DMT	\$	88.72
Smelting \$/DMT	\$	75.00
Smelter recovery %		96.5%
Refining \$/lb	\$	0.08
Gold Processing		
Mill recovery %		47%
Smelter payable %		95%
Refining \$/oz	\$	6.00
Process cost with G&A \$/DMT	\$	3.90
Mining \$/DMT	\$	0.89
	•	_
Copper price \$/lb	\$0.6	5-\$1.50
Gold price \$/oz		\$400
		050 400
Overall pit slope angles		35°-42°
DMT = Dry Metric Tonne		
WMT = Wet Metric Tonne		

1.7 Recommendations

MDA and Sivertz believe that Mirador is a property of merit. For Mirador specifically, it is recommended that certain work on the resource be completed:

- Make paper cross sectional interpretations through the Mirador deposit that describe and define the rock types, material types, alteration zones, and structure;
- Continue work on the solids using the previously mentioned geologic sections to guide the definition of the rock and material types, and modify the model through various iterations of slicing and reinterpretation;
- With the new material type and rock type models completed, estimate resources using a partial-block model to replace the sub-block model; and
- Estimate zinc grades.

Estimated costs for the previously described resource modeling work would be approximately \$100,000.



In addition, engineering, cost estimation, and environmental/social baseline work should be continued, in order to update the Feasibility Study completed by AMEC Americas Limited. This should involve:

- A review of the proposals received for mine engineering, procurement and construction.
- Studies to determine the optimum production capacity for the Mirador Project, balancing constraints such as availability of electrical power and other logistical realities against maximum achievable mining and milling rates.
- Preparation of an overall mine plan to accommodate expansion to a range of milling capacities from 25,000 tpd to 50,000 tpd.
- Preparation and review of capital expenditure and operating costs for the optimum mine expansion plan.
- Complete the ongoing slope stability work.
- Additional metallurgical test work to verify that there are not changes to metallurgical characteristics at depth.
- Identify any potential issues relating to large waste dumps and tailings facilities. Estimated costs for the previously described engineering work would be approximately \$150,000.

Continued permitting, environmental baseline studies, planning, and pre-production work are all justified. It is further recommended that the nearby Mirador Norte copper deposit should be evaluated from a resource standpoint.



2.0 INTRODUCTION AND TERMS OF REFERENCE

2.1 Introduction

Corriente Resources Inc. ("Corriente") engaged Mine Development Associates ("MDA") to provide an updated mineral resource estimate for its Mirador Project in southeastern Ecuador. The work entailed estimating mineral resources in compliance with the CIM Mineral Resource and Mineral Reserve definitions referred to in National Instrument ("NI") 43-101. The work also involved the preparation of a Technical Report as defined in NI 43-101 and in compliance with the format set out in 43-101F1. Steven Ristorcelli, P.Geo., Principal Geologist for MDA, served as the Qualified Person responsible for preparing the resource estimate. Scott Hardy, MDA, is the Qualified Person for estimating the in-pit resources. John Hoffert P.Eng. of Hoffert Processing Solutions Inc. is the Qualified Person for metallurgy. This Technical Report was prepared by Steven Ristorcelli, Scott Hardy of MDA, and George Sivertz, P.Geo., Senior Geologist, OreQuest Consultants Ltd., and John Hoffert P.Eng. of Hoffert Processing Solutions Inc. Steven Ristorcelli visited the Mirador property from January 4 to January 7, 2005. John Hoffert visited the Mirador property from May 1, 2006 to May 3, 2006. George Sivertz has not been to the Mirador property.

The MDA work represents a significant change in the level of confidence of the mineral resource since the last resource disclosure on this deposit, which appeared in a Technical Report on the Mirador Project, dated November 2004 (AMEC 2004). In that report, AMEC estimated Indicated Resources totaling 309,700,000 tonnes grading 0.66% Cu and 201 parts per billion (ppb) gold, at a 0.4% Cu cutoff. Inferred resources, also at a 0.4% Cu cutoff, were reported to be 315,100,000 tonnes grading 0.56% Cu and 170 ppb gold. Silver grades were not reported. In its 2005 study, MDA reported Measured and Indicated resources of 437,670,000 tonnes grading 0.61% Cu, 190 ppb gold, and 1.5 ppm silver at a 0.4% Cu cutoff grade. Inferred resources, also at a 0.40% Cu cutoff, were reported to be 235,400,000 tonnes grading 0.52% Cu, 170 ppb gold, and 1.3 ppm silver.

2.2 Terms of Reference

MDA and Sivertz are not associated or affiliated with Corriente Resources Inc, Ecuacorriente S.A., Minera Curigem S.A., Minera Panantza S.A., or any related companies. Any fees paid to MDA or Sivertz for the work done or preparation of this Technical Report are not dependent in whole or in part on any prior or future engagement or understanding resulting from the conclusions of this report. The fees are in accordance with industry standards for work of this nature.

MDA completed a NI 43-101-compliant resource estimate for the Mirador deposit in 2005, and also conducted pit optimization studies, and a review of the quality assurance/quality control procedures used by Corriente in the 2005 drilling program at Mirador. The sections of this report that discuss these studies (Sections 14, 17, and the pertinent sections of the Summary, Conclusions, and Recommendations) are based on the work done by MDA in 2005.



The sections of this report that discuss other aspects of the Mirador project rely on information set out in the following reports:

- AMEC Americas Limited, 2005: Mirador Copper Project Feasibility Study Report. May 2005.
- Dawson, J.M., and Makepeace, D.K, 2003: Mirador Project, Corriente Copper Belt, Southeast Ecuador. Order-of-Magnitude Study, Part 1, Technical Report. February 2003.
- Lomas, S., 2004: Technical Report, Mirador Project. Zamora-Chinchipe Province, Ecuador. AMEC Americas Limited Technical Report prepared for Corriente Resources Inc, October 22, 2004.
- Makepeace, D.K, 2001: Corriente Copper Belt Project, Southeast Ecuador, Order-of-Magnitude Study (Preliminary Assessment Technical Report), June 22, 2001.
- Makepeace, D.K, 2002: Mirador Project, Corriente Copper Belt, Southeast Ecuador. Preliminary Assessment Technical Report, February 12, 2002.
- Makepeace, D.K, 2002: Mirador Project, Corriente Copper Belt, Southeast Ecuador. Preliminary Assessment Technical Report, September 3, 2002.
- P&T Asesores Legales, Abogados 2005: Letter Regarding Certain Corporate Matters and the Status of Title to the Mining Concessions in Ecuador. Prepared for Corriente Resources Inc, December 29 2005.

The report is also based in part on personal communications with Mr. Ken Shannon, P. Geo., Chairman and C.E.O. of Corriente Resources Inc, Mr. John Drobe, P.Geo., geologist for Corriente, and other field geologists who worked at Mirador in 2005. It also draws on information provided in other legal, geological and technical reports listed in the References section of this report. The writers have reviewed all of the information provided by Corriente and believe the information to be reliable.

All measurement units used in this report are metric, and currency is expressed in US dollars unless stated otherwise. The coordinate system in use on the property and in all maps and references in this report is UTM zone 17 S, datum Provisional SAD 1956. The estimated costs in the Recommendations sections (1.6 and 21.0) include Ecuadorian taxes where applicable.



3.0 RELIANCE ON OTHER EXPERTS

MDA and Sivertz have not personally reviewed the land tenure, are not Qualified Persons or experts with regard to land tenure in Ecuador, and have not independently verified the legal status or ownership of the properties or underlying option agreements. The law firm of P&T Asesores Legales, an independent law firm contracted directly by Corriente, provided the writers with legal opinions on land tenure, environmental liabilities, and the status of permits. All metallurgical information and reporting are adapted or quoted verbatim from information published in reports by AMEC (2004, 2005).

The summaries of the Mirador Project environmental and social baseline studies in this report are based on information stated in the report titled "Mirador Copper Project <u>Feasibility Study Report</u>", dated May 2005 (AMEC Americas Limited).

The results and opinions expressed in this report are conditional upon the aforementioned environmental, geological and legal information being current, accurate, and complete as of the date of this report, and the understanding that no information has been withheld that would affect the conclusions made herein. The writers reserve the right, but will not be obliged, to revise this report and conclusions if additional information becomes known to them subsequent to the date of this report.



4.0 PROPERTY DESCRIPTION AND LOCATION

4.1 Property Location

The Mirador property is centered 10 km east of the Rio Zamora (Zamora River) in the Zamora-Chinchipe Province of southeast Ecuador, adjacent to the border with Perú (Figure 4.1). The concessions are approximately 340 km south of Ecuador's capital city of Quito and 70 km east-southeast of the city of Cuenca.

The center of the Mirador concession group has UTM coordinates 9,604,200 N and 785,000 E (UTM Zone 17S, Provisional South American Datum 1956). The six concessions are contiguous and cover an area of 13,640 hectares. The claims are registered with the National Directorate of Mining and have not been legally surveyed.

MDA and Sivertz are not aware of any historic mine workings or tailings within the Mirador mineral concessions.

4.2 Mineral Tenure

Billiton Ecuador, now BHP Billiton ("Billiton") began exploration in southeastern Ecuador in 1994 and identified a number of possible porphyry copper targets in the region. In April 2000, Billiton and Corriente entered into an agreement covering 230 sq km of mineral concessions in the southern part of the region, including the area of the Mirador property. Under the agreement, Corriente could earn a 70% interest in each of the Billiton projects by completing a feasibility study and meeting certain financial and work commitments. At the completion of each feasibility study, Billiton could elect to back-in for a 70% interest by providing production financing, retain a 30% working interest, or dilute to a 15% Net Profit Interest ("NPI").

Corriente also entered into an exploration management arrangement where Lowell Mineral Exploration ("Lowell") could earn up to 10% of Corriente's interest in certain properties in exchange for managing the exploration of the properties.

In December 2002, Corriente announced that it had received notice from Billiton that the Mirador property was to be separated from the existing copper-gold joint venture in Ecuador, and that the exploration concessions were to be transferred to Corriente. Billiton was to retain no back-in rights, but had the option to retain its 30% participating interest in Mirador or revert to a 2% Net Smelter Royalty ("NSR"). Billiton elected to revert to the 2% NSR interest. At this time, Lowell held a 10% interest in Corriente's Mirador project. Corriente, in December 2003, granted Lowell the option to exchange its 10% interest in the Corriente mineral concessions, including Mirador, for a 100% interest in the Warintza property. In June 2004, Lowell exercised that option. Corriente, through its wholly-owned subsidiary companies in Ecuador, now holds a 100% interest in the Mirador property. BHP Billiton holds a 2% NSR interest in the Mirador deposit.



Figure 4.1 Location Map COLOMBIA PACIFIC **OCEAN** Equator 0° ECUADOR CORRIENTE Guayaquil COPPER BELT PANANTZA SAN CARLOS DEPOSITS Cuenca Puerto Morono Machala (Puerto Bolivar) Gualaquiza
Proposed
Concentrate Trucking PERU Route 4° S Loja **MIRADOR DEPOSIT** South SCALE Miles Pacific Ocean Atlantic Ocean 70 Kilometers 0 **PROJECT** 78° W LOCATION MAP

March 2004



The location of the six individual concessions that make up the Mirador property is shown in Figure 4.2 and Figure 4.3. The state code numbers, area in hectares, property registration dates and ownership of the Mirador concessions are as indicated in Table 4.1 (P&T Asesores Legales 2005). The companies listed in Table 4.1, Ecuacorriente S.A. and Minera Curigem S.A., are fully owned by Corriente (P&T Asesores Legales 2005; Appendix A). According to information supplied by Corriente, the Mirador deposit is located along the boundary between the Mirador 1 and Mirador 2 concessions.

The concessions cover an area of 13,640 hectares (13.64 sq km). All the concessions are within Zamora-Chinchipe Province.

According to Ecuadorian Mining Law, concessions registered against title to mining properties have a term of 30 years, which can be automatically renewed for successive 30-year periods, provided that a written notice of renewal is filed by the registered concession holder before the expiry date (P&T Asesores Legales 2005).

Table 4.1 Mirador Concession Locations and Areas (Data from Corriente and P&T Asesores Legales 2005)

Concession	Code	Hectares	Owner	Registration Date
	number			
Mirador 1	500807	2,400	Ecuacorriente S.A.	February 7 2003
Mirador 2	500805	1,200	Ecuacorriente S.A.	February 7 2003
Curigem 18	4768	1,600	Minera Curigem S.A	August 23 2001
Curigem 18 este	500806	800	Ecuacorriente S.A.	February 7 2003
Curigem 19	4769	2,900	Minera Curigem S.A	August 23 2001
Caya 36	500200	4,740	Minera Curigem S.A	August 23 2001



Figure 4.2 Concession Location Map

(from Corriente)

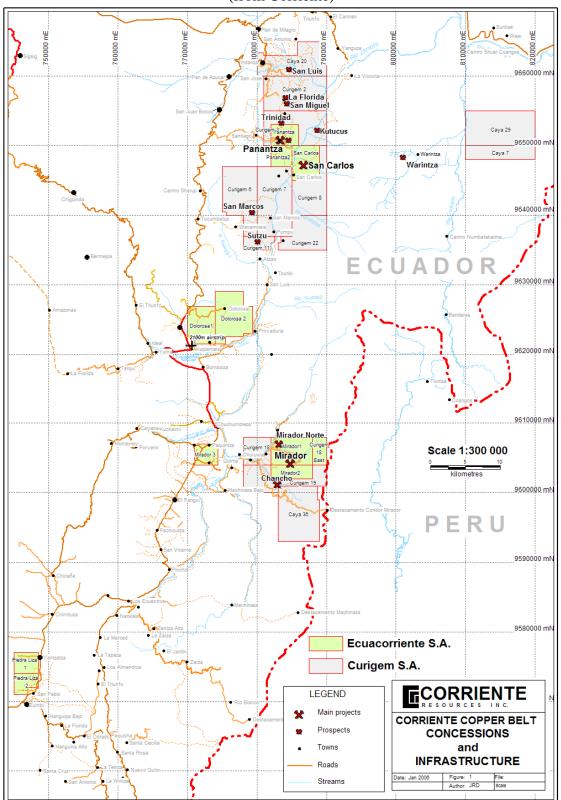
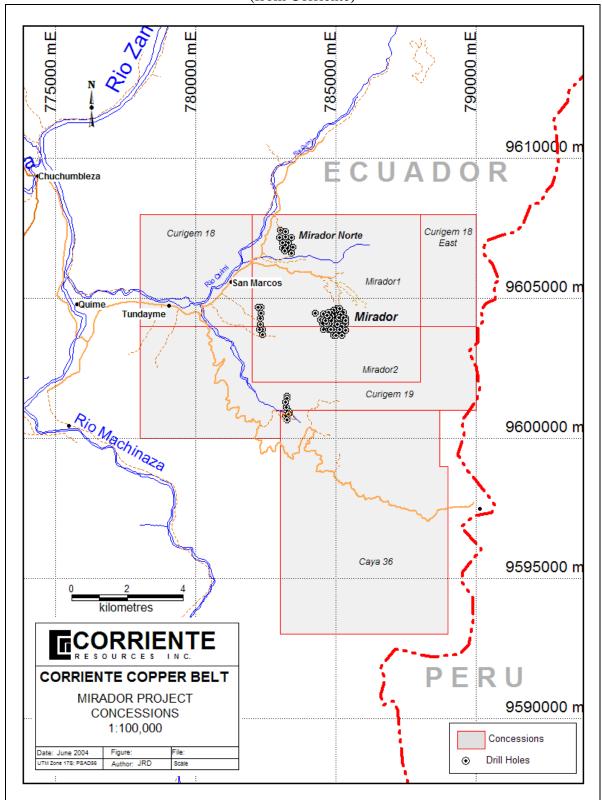




Figure 4.3 Detailed Map of the Mirador Concessions

(from Corriente)





Each year, owners of mining concessions in Ecuador must pay an "annual conservation patent fee" for each hectare of area that is covered by their concessions. The fees are payable during the month of March. When the appropriate fees are paid, the registration of each concession is renewed in the name of the present holder for another one-year term. The patent fees are shown in Table 4.2 table below (P&T Asesores Legales 2005). According to Corriente, the six Mirador concessions are currently in good standing with respect to the payment of the conservation patent fees; the next payments are due in March 2006.

Table 4.2 Annual Conservation Patent Fees Payable For Mineral Concessions In Ecuador

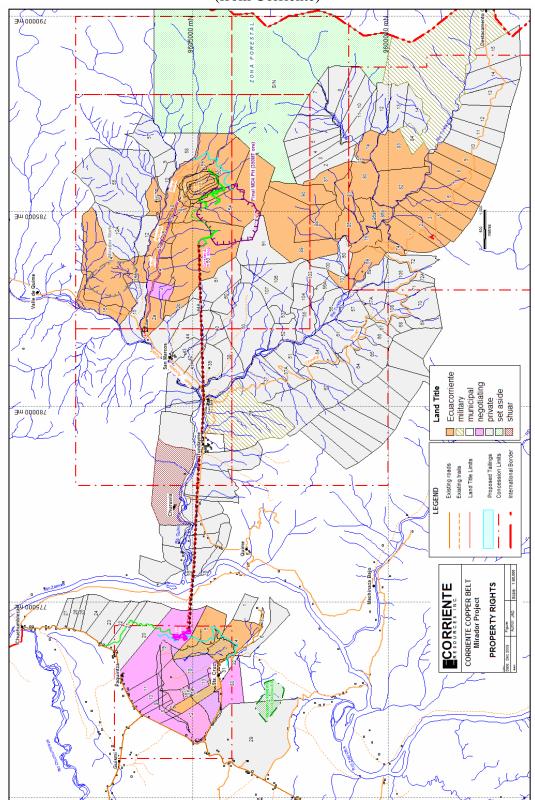
From (Year of Registered Ownership)	To (Year of Registered Ownership)	Conservation Patent Fee per hectare per year (US\$)
First	Third	1.00
Fourth	Sixth	2.00
Seventh	Ninth	4.00
Tenth	Twelfth	8.00
Thirteenth	Onwards	16.00

Corriente has acquired copies of the land maps that show the surface rights holdings in the Mirador area (Figure 4.4). The surface rights for all land that may be affected by proposed mining, construction sites, dumps and other infrastructure needed for the Mirador project have been purchased by Corriente, or are in the process of negotiation for purchase, or are being registered and verified. Figure 4.4 illustrates the status of surface rights acquisition. The different colors show the status of the surface rights. Gray represents areas with independently owned surface rights, and pink indicates areas that have been purchased by Corriente. The areas that are in the process of being negotiated or acquired by Corriente are shown in magenta.



Figure 4.4 Detailed Map of the Mirador Property Rights

(from Corriente)





4.3 Permits and Agreements

For the exploration phase of the Mirador property, all the required permits are included in the approved exploration-phase Environmental Impact Assessment ("EIA") that is on file with the Ecuadorian Government. For any mine development, an EIA report must be filed and approved by Government authorities.

The Mirador mining EIA and all supporting documents were submitted to the Ministry of Energy and Mines in Quito, Ecuador, in December 2005. The EIA covers both the environmental aspects of proposed mining operations at Mirador, and community and social plans associated with the Mirador project (Corriente Resources News Release dated December 20, 2005). A list of required permits is presented in Table 4.3.

The following discussion of the Ecuadorian environmental permitting and approval process, including Table 4.3, is quoted *verbatim* from the report titled "Feasibility Study Report, Mirador Project, Ecuador", by AMEC Americas Limited (AMEC 2005).

The Mirador project is located within the Cordillera del Condor. This area is considered ecologically important because of its high biological diversity and presence of endemic species.

Ecuador's environmental legislation is extensive and their requirements for early stage operations i.e., exploration, are well defined. Ecuador is one of the few Latin American countries that have adopted an EIA process for exploration activities. Argentina, Chile, and Peru have adopted a similar process to conduct environmental assessments for early stage exploration.

Under Ecuadorian Mining Law, the Ministry of Energy and Mines handles the environmental approval system for new mining projects. Mining concession holders are required to complete environmental impact studies and environmental management plans to prevent, mitigate, rehabilitate, and compensate for environmental and social impacts as a result of their activities. These studies are approved by the Ministry of Energy and Mines Sub secretary of the Environment.

Terrambiente, a Quito-based environmental firm, has completed an environmental baseline assessment for the Mirador Project. Baseline data collection commenced in March 2004 and has been ongoing through the study period.

The environmental approval process is summarized as follows:

- Proponent files a Project Description and Terms of Reference (ToRs) regarding how the EIA will be developed with respect to the conditions within the project area as well as the project description with the Ministry of Energy and Mines (MEM) and Ministry of the Environment (MoE). The ToR for Mirador has been reviewed by MEM and MoE.
- These ToRs need to be approved by MEM and published.
- Environmental baseline studies and environmental impact assessment are completed by proponent in accordance with the ToR.



- The EIA is presented to the local affected communities and input to the EIA is requested. Corriente will have community meetings in Valle del Quimi, San Marcos, Tundayme, El Pangui, and at the Ministries of Energy and of the Environment. The EIA is updated to acknowledge community input.
- The EIA is submitted to MEM who reviews within a 45-day period after which the ministry will request Corriente to respond to any comments and questions regarding the EIA.
- Corriente will have a 30-day period to submit responses to all comments and questions.
- The MEM will then take another 30-day period to revise the documentation and pronounce its satisfaction with all information, obtaining in this way the Approval for the EIA.
- Once the EIA is approved, proceedings towards granting of the Environmental License starts. It is estimated that another 30-day period is needed to prepare and grant the Environmental License.
- Submission of EIA to the Ministry of the Environment will take place at the same time as with the Ministry of Energy and Mines. Approval times are expected to be less than MEM.

Table 4.3 List of Major Permits required for the Project (AMEC 2005)

Permit	Granting Institution	Requirements	Estimated Time for Approval
Environmental	Ministry of Energy and	Approval of EIA by	30 days after approval of the
License (EIA)	Mines/ Ministry of	both Ministries.	project and payment
	Environment	Payment of license	
		fees.	
Permit to	Ministry of Environment	Approval of EMP,	Valid for two years. To be
Discharge		payment of fees,	obtained after one year of
		compliance with EMP	operations. Estimated time to
		and regulations.	obtain the permit: is 30 days.
Permit to Modify	National Council for		
Water Courses	Hydrological Resources	_	
	(Consejo Nacional de	_	-
	Recursos Hídricos)		
Permit to Use	Joint Command of Logistics	Compliance with safety	
and Transport	Management/Naval and Air	regulations	
Explosives	Zone Command Squad		
	(Dirección de Logística del		-
	Comando Conjunto/		
	Comandos de Brigada y de		
	las Zonas Naval y Aérea)		
Health and	Ministry of Labor	Presentation of	Estimated time to obtain the
Safety Permit		Company's Heath and	permit is 30 days.
		Safety Plan.	

As a note to Table 4.3, Corriente announced that the Mirador copper project Environmental Impact Assessment (EIA) met all the legal requirements of the Ecuadorian Ministry of Energy and Mining and approval has been granted on the EIA (Corriente news release, May 4, 2006).



4.4 Environmental Impact Assessment

MDA and Sivertz are not aware of any environmental factors that could negatively affect the development of this project. The firm of Terrambiente, a Quito-based environmental firm, has completed an environmental baseline assessment for the Mirador project (AMEC 2005). Baseline data collection commenced in March 2004 and has continued since that time. The following activities, related to ongoing environmental studies, were conducted throughout 2005 at the Mirador property:

- Weekly measurements are collected from five vibrating wire piezometers installed in drill holes in 2004.
- Rainfall data are collected from two automated tipping rain buckets, one located on the deposit itself, and the other located one kilometer to the north.
- Complete weather data are collected by manual and automated means from a weather station located in the Mirador camp.
- Automated water level, manual staff gauge, and total solids measurements are taken from five stations located at various points around the deposit.
- Water quality samples are collected from three streams draining the deposit; there are another 16 regional sample points outside the area of mineralization.



5.0 ACCESS ROUTES, CLIMATE, PHYSIOGRAPHY AND INFRASTRUCTURE

5.1 Access Routes

Access to the Mirador property from Quito, the capital city of Ecuador, can be gained by road or by a combination of air and road travel. There is scheduled air service from Quito to Cuenca and Loja, the cities northwest and southwest of the property. From these centers, small aircraft can be chartered to fly to Gualaquiza, the nearest airfield to the deposit.

There is road access from Quito to Cuenca for the transport of samples or heavy equipment. A system of gravel roads from Cuenca leads to the village of Tundayme, 6 km from the project site. The road distance is approximately 230 km and the travel time is about five to six hours. There is also road access from Tundayme to the Pacific Ocean port of Machala.

Corriente constructed a six-kilometer pilot road in 2005, to access the east side of the Mirador deposit. Short trails from the end of this road provide access to most of the critical sectors of the project area.

5.2 Climate

The area has a wet equatorial climate with a reported rainfall of 2,300 millimeters (mm) per year. Rainfall can exceed 60 mm in a 24-hour period. Variations in the local terrain exert a strong influence over rainfall, so the area has many different local rain regimes. Fieldwork is possible all year round. The best time for airborne surveys or road and trail construction is from October to December, because of clearer skies and drier weather conditions.

5.3 Physiography

Tributaries of the Rio Zamora drain the central and western parts of the Mirador property. The flanking highland areas of the Paramos de Matanga on the west, and the Cordillera de Condor on the east, rise to maximum elevations of 4,200 and 3,500 meters above sea level (masl), respectively. The elevations of the property range from about 800 to 1,400 masl. The property supports second-growth tropical forest, although there are numerous clearings at lower elevations.

5.4 Infrastructure

The infrastructure within the immediate area of the Mirador property is shown in Figure 4-2. The Mirador exploration camp is supplied with electricity from the local power grid.

It is predicted that the Ecuadorian electrical power grid will not be able to supply sufficient power to meet the future needs of the Mirador project, which for the present mining plan are estimated to be 28.3 megawatts. In order to secure a supply of electrical power, Corriente has purchased the rights to the Sabanilla Hydroelectric Project in Ecuador, including all permits, studies and designs completed to date. The Sabanilla Hydroelectric Project is located in southern Ecuador, in the Province of Zamora Chinchipe, 40 km east of the city of Loja. A 95-km long transmission line (138 kilovolts) will be



needed to reach the Mirador site from the Sabanilla substation. It is expected that the Sabanilla Project will be able to supply an average of approximately 23.5 MW of power to the mine, and the remainder is to come from the Ecuadorian electrical power grid (AMEC 2005).

According to a Corriente news release on March 22, 2006, Corriente signed a "Letter of Intent (LOI) with Hidroabanico S.A. to supply the 28.5 MW power needs of proposed mining operations at the Mirador copper-gold project. The terms outlined in the LOI propose a 10 year Power Purchase Agreement (PPA) with a proposed rate of \$0.05/kWh. The Hidroabanico facility has already been completed to a 15 MW stage and an expansion is under way to the final size of 37.5 MW, with completion slated for December 2006. The Hidroabanico facility is a run-of-river design and provides "green" energy that qualifies for the carbon credit program. The energy will be delivered through a dedicated line to the mine, which will cost in the order of \$US10 Million to construct and will be included in the capital cost estimate for Mirador. As part of the LOI, Hidroabanico will have the first right of opportunity to provide energy needs for the planned 25,000 tpd to 50,000 tpd expansion at Mirador. A due diligence review is presently underway at the site, which will be followed by final negotiation of the PPA."

The closest existing airstrip is at Gualaquiza, about 40 km to the northwest of the deposit. It has an asphalt runway approximately 2,075 m long (AMEC, 2004). The availability and sources of water, mining personnel, potential tailings storage areas, potential waste disposal areas and processing plant sites are discussed at length in the May 2005 Feasibility Study Report (AMEC 2005).



6.0 HISTORY

6.1 Exploration History

Billiton Ecuador ("Billiton") began regional exploration in southeastern Ecuador in 1994. Stream-sediment sampling was the main tool used to locate base metal anomalies. After further follow-up and mapping, Billiton identified possible porphyry copper systems associated with these anomalies. At least eight separate porphyry copper systems have now been identified in the region (AMEC 2004).

The area of the present Mirador property attracted interest during the original reconnaissance geological and geochemical surveys completed in December 1994. These surveys, which included the collection of 315 stream sediment pan concentrate samples, identified a 50 sq. km drainage area where stream sediments contained anomalous grades of Cu, Mo, Au, Zn, and Ag. During the period from 1995 to 1999, Billiton was forced to restrict its activities to the north part of the region, away from the Peruvian border. A large area in the Cordillera del Condor, including the Mirador property, was declared off limits by the Ecuadorian Government during the time of the border conflict between Ecuador and Perú.

After Ecuador and Perú signed a peace treaty in July 1999, Billiton completed detailed follow-up surveys to better define the anomalous areas at the Mirador property. Billiton collected 746 soil samples along ridges and 219 rock chips from outcrops in stream drainages traversing the anomalous zones. This work, along with geological mapping, defined the Mirador anomalous zone. In April 2000, Billiton and Corriente entered into an agreement covering the area of the Mirador property.

In February 2002, after the completion of 52 diamond drill holes at Mirador, Corriente published the results of a mineral resource estimate (Makepeace, February 2002). The estimated tonnage and grade, calculated at a 0.65% Cu cutoff grade, were 218 Mt grading 0.73% Cu, all in the Inferred Mineral Resource category.

In February 2003 Corriente published the results of another mineral resource estimate based on the 62 holes completed at Mirador (Dawson and Makepeace, 2003). The estimated tonnage and grade, calculated at a 0.65% Cu cutoff grade, were stated as 182 Mt grading 0.76% Cu, all in the Inferred Mineral Resource category. An average gold grade of 0.22 g/t was reported to accompany this copper resource.

In July 2003, Sumitomo of Japan completed independent metallurgical tests, with favourable results. AMEC reviewed this work and found it to be done to industry standard. Subsequent follow-up work has confirmed its conclusions (AMEC 2004). The metallurgy of the Mirador mineralization is discussed in more detail in Section 16 of this report.

A fourth phase of drilling was conducted at Mirador between December 2003 and April 2004. A total of 8,091 m of core drilling was completed in 29 holes.



In November 2003, Corriente commissioned AMEC Americas Limited ("AMEC") to be the primary consultant for the preparation of a bankable feasibility study for the Mirador Copper Project. Knight Piésold Ltd was responsible for the design of a Tailings Management Facility and related infrastructure, and Merit Consultants International Inc. provided study coordination, project planning and scheduling and capital cost estimates. The Feasibility Study Report was completed in May 2005.

In 2004, Corriente engaged AMEC to provide a mineral resource estimate and Qualified Person's review and Technical Report for the Mirador Project. The work entailed estimating mineral resources in conformance with the CIM Mineral Resource and Mineral Reserve definitions referred to in National Instrument ("NI") 43-101, Standards of Disclosure for Mineral Projects. It also involved the preparation of a Technical Report as defined in NI 43-101 and in compliance with the format set out in 43-101F1. Susan Lomas, P.Geo., an employee of AMEC, served as the Qualified Person responsible for preparing the resource estimation. The mineral resource estimate, based on data from the 91 core holes completed as of April 2004, was used in the preparation of the Feasibility Study Report. The details of the mineral resource estimate are set out in this report, in the section titled "2004 Mineral Resource Estimate (AMEC)".

This historic mineral resource estimate is superseded by a more recent estimate (MDA 2005), both prepared in compliance with National Instrument 43-101 and CIM definitions, using 3-D geological-mining software.

Corriente conducted 11,935 m of core drilling in 2005. Much of this 52-hole program involved the drilling of angled infill drill holes that were intended to better define the early porphyry dikes, which account for most of the lower-grade zones in the deposit, and post-mineral dikes. A six-kilometer pilot road was pushed through to the east side of the deposit from the existing access road leading south from the camp, creating better access to the drill platforms.

In the fourth quarter of 2005, Corriente retained MDA to prepare an updated mineral resource estimate and to conduct pit optimization studies followed by a reserve estimate. The purpose of the mineral resource estimate update was to incorporate the new data from the fifty-two new drill holes completed in 2005 into the resource model. MDA relied upon the results of previous work, and, unless there were compelling reasons to do otherwise, used procedures similar to those used by AMEC in the preparation of the 2004 mineral resource estimate (AMEC 2004).

6.2 2004 Mineral Resource Estimate (AMEC)

The mineral resource for the Mirador deposit was estimated under the direction of Susan Lomas, P.Geo., of AMEC. The estimate was made from a 3-dimensional block model utilizing commercial mine planning software (Gemcom®). Pertinent parts of the report titled "Technical Report, Mirador Project, Morona Santiago Province, Ecuador" (AMEC (2004) are extracted *verbatim*.

Geologic models were created of the dikes and the supergene units. AMEC checked the shapes for interpretational consistency on section and plan, and found them to have been properly constructed. To



constrain grade interpolation in each of the zones, AMEC created 3-dimensional mineralized envelopes based on copper and gold grades. These were derived by a method of Probability Assisted Constrained Kriging (PACK) to initially outline a general shape. The threshold grade for Au was 0.2 g/t and for Cu it was 0.5%.

The data analyses were conducted on original and 6 m composited assay data. AMEC reviewed the compositing process and found it to have been performed correctly. Detailed data analysis indicated the domaining and tagging of the assay and the composite data functioned well.

Extreme grades were examined for copper and gold composite values. Cu grades had a smooth distribution with few extreme grades. Gold showed extreme grade values and a grade cap of 0.60 g/t was imposed on the assay data prior to grade interpolation.

Variography was completed for gold and copper on composite data from the main mineralized unit within and outside the grade probability shells. Only hypogene material was investigated. The copper correlograms showed ENE-WSW trending, steeply dipping structures while the gold correlograms showed NS trending, subvertical structures.

Values for copper, capped and uncapped gold, and bulk density were interpolated into the block model using ordinary kriging (OK), inverse distance weighting to the eighth power (ID8) and the nearest-neighbour (NN) methods.

AMEC completed a review of the Mirador resource block model. The model was checked for proper coding of drill hole intervals and block model cells. Gold and copper grade interpolation was examined relative to drill hole composite values by inspecting the sections and plans. The checks showed good agreement between drill hole composite values and model cell values.

AMEC checked the block model estimates for global bias by comparing the average copper and gold grades from the model ID8 with means from OK and NN estimates. The results show no evidence of bias in the estimate.

AMEC checked for local trends in the grade estimates by plotting the results from the OK, ID, and NN estimate results on easting, northing and elevation swath plots. The results for copper and gold grade inside the grade probability shells show close tracking between the three estimates and no local trends.

The final check performed, was to check the model for smoothing through the Discrete Gaussian or Hermitian polynomial change-of-support method described by Journel and Huijbregts (Mining Geostatistics, Academic Press, 1978). The grade-tonnage predictions produced for the model show that grade and tonnage estimates are validated by the change-of-support calculations over the likely range of mining grade cutoff values (0.4% to 0.6% Cu).

The mineral resources of the Mirador project were classified using logic consistent with the CIM definitions referred to in National Instrument 43-101. The project mineral resources were classified as



either Indicated or Inferred Mineral Resources. [Table 6.1] contains the results of the resource estimation for the Mirador Deposit as of 23 September 2004. The resource estimate result for Mirador is being declared using the 0.40 %Cu cutoff. The resources are reported to a depth of 850 m elevation, which is approximately 500 m below the surface. Preliminary open pit planning work, conducted as part of an ongoing Feasibility Study, has shown potential open pit bottoms to be around 1000 m elevation, 150 m above the deepest interpolated grade blocks.

Table 6.1 Mirador Deposit Mineral Resource Summary – 23 September 2004

			Au	Cu
	Zone	Tonnes	(g/t)	(%)
(0.4 Cu % Cutoff			
Indica	ted Mineral Resource			
	Mixed	1,300,000	0.23	0.57
	Enriched	6,700,000	0.24	0.99
	MNZD	301,700,000	0.20	0.65
Totals	Indicated Hypogene	301,700,000	0.20	0.65
	Indicated Supergene	8,000,000	0.24	0.92
Inferi	red Mineral Resource			
	Mixed			
	Enriched	1,200,000	0.25	0.83
	MNZD	313,900,000	0.17	0.56
Totals	Inferred Hypogene	313,900,000	0.17	0.56
	Inferred Supergene	1,200,000	0.25	0.83



7.0 GEOLOGICAL SETTING

7.1 Regional Geology

The copper-gold-silver mineralization of the Mirador deposit is hosted by Late Jurassic granite and porphyries of the Zamora Batholith. This batholith is one of a number of Jurassic intrusions in the Cordillera Real and sub-Andean regions of Ecuador that have been mapped as members of the Abitigua Subdivision. Isotopic age dates for the younger Late Jurassic porphyry intrusive phases of the Zamora Batholith range from 152 to 157 Ma.

To the south of the Mirador deposit, quartz sandstone of the Cretaceous Hollin Formation forms 50-m to 80-m high cliffs. This resistant unit unconformably overlies the Jurassic intrusive rocks of the Zamora batholith and covers the southern limits of the Mirador alteration/mineralization complex.

7.2 Local and Property Geology

The Zamora batholith forms the wall rocks of the Mirador porphyry copper-gold system. Within the mineralized zone, the intrusion comprises mainly equigranular Zamora granite/granodiorite, with some minor leucogranite dikes along the west and southwest margins, and rare diabase dikes up to two meters in width. In drill core the Zamora granite appears highly fractured; this is a weathering effect and is due to the dissolution of anhydrite and gypsum from veinlets. Where anhydrite is unaltered by weathering and leaching, the drill core is relatively competent. A typical cross section of the Corriente model that helps to illustrate the following geological discussion is presented in Figure 7.1.

The oldest porphyritic rocks that intrude Zamora granite within the limits of the Mirador deposit are trachytic hornblende-feldspar dikes ("Jefp"), which strike north and east. A dike in the southern part of the deposit appears to be slightly older than the northern dikes, based on its degree of mineralization. In highly altered zones and in leached surface exposures, the porphyritic dikes are distinguished from the Zamora granite mainly by their large hornblende phenocrysts and equant feldspar crystals.

Near the center of the mineralized system is a large vertical diatreme of breccia ("brmn", not shown in Figure 7.1 but parallels and is inside of the mineralized zone), composed of angular fragments of the early porphyry dikes, Zamora granite, and quartz-vein fragments. The early porphyry dikes can be traced into the breccia but the brecciation obscures the contacts between the granite and early porphyry. The breccia is mostly fragment-supported, and the matrix consists of rock flour and fine rock and vein fragments. The matrix also contains sulfide-filled vugs, which, together with the quartz-vein fragments, allow mapping of the unit in weathered surface exposures. Fragments are angular to sub-angular and show potassic alteration.

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Northeast-striking, northwest-dipping hornblende-feldspar porphyry dikes ("Jhbp") cut the breccia and the wall rocks of the deposit. Based on their degrees of alteration and mineralization, these dikes are believed to have relative emplacement ages ranging from syn-mineral to post-mineral. These dikes are larger and more numerous along the southeast and northwest margins of the mineralization. A quartz-rich variety appears to be the youngest in the series. These rocks are sparsely fractured relative to the mineralized rocks and lack any quartz veining or high-temperature alteration. Outcrops are blocky and resistant and weather to a characteristic bright red clay due to the oxidation of abundant magnetite.

The youngest rocks are post-mineral hydrothermal breccia dikes and irregular diatremes ("brpm"). These intrusive breccias are characterized by a polymictic clast assemblage of mineralized and unmineralized rock, the relative quantity of each clast type being dependent on whether the breccia intruded mainly mineralized rocks, or post-mineral intrusions. The matrix is finely ground rock; in some places the matrix also contains milled sulfide minerals. The breccia dikes and diatremes seem to have preferentially intruded post-mineral dikes. They are most common along the southeast margin of the deposit. Intrusive breccia also occurs as irregular plugs around the north and northeast margins of the mineralized zone. Copper grades within the intrusive breccia range from very low to slightly less than the deposit average, depending on the amount of mineralized rock incorporated. Outcrops of this breccia are massive and very sparsely fractured. In drill core, the breccia is the least fractured lithology in the deposit.



Figure 7.2 Drill Core Photo of DDH M64 Showing Low RQD



Figure 7.3 Drill Core with Unaltered Anhydrite (Below the Gypsum Front)





8.0 DEPOSIT TYPES

The host rock, alteration, and mineralization at the Mirador deposit are characteristic of a calc-alkaline porphyry copper system. Copper deposits of a similar style are widespread in the Cordilleras of North and South America.



9.0 MINERALIZATION

The sequence of mineral deposition at Mirador has been divided into early-stage molybdenum, early-stage copper \pm gold, and late-stage copper + gold events, with a final weak polymetallic vein stage. Both copper-gold depositional events are dominated by chalcopyrite, with traces of native gold.

Molybdenite is present in systems of early-stage quartz veins that have a preferred east-west orientation. These veins occur as stockwork in both Zamora granite and early porphyry dikes.

Early copper-gold mineralization occurs as finely disseminated chalcopyrite (with traces of native gold), associated with pervasive potassic alteration (mainly as secondary biotite). The later copper-gold event postdates the emplacement of the central breccia diatreme. This mineralization is characterized by abundant disseminated chalcopyrite in texture-destructive potassic alteration zones in the granite and early porphyry, and as coarse disseminations and centimeter-size intra-clast blebs in the central diatreme breccia. Mineralization is generally less abundant in the early porphyry dikes because either they were not as receptive to mineralizing fluids as the granite, or they were emplaced slightly after the peak of the early copper-gold mineralization phase. However, the southernmost early porphyry dike is just as strongly mineralized as the Zamora granite.

A third and minor mineralized event is manifested by subvertical, widespread, sparsely distributed polymetallic sulfide veins that are less than five centimeters in width. The veins include several varieties, ranging from massive pyrite veins with elevated gold grades to massive chalcopyrite-pyrite-sphalerite veins with elevated silver, zinc, copper and gold grades. These veins cut the youngest of the late-stage porphyry dikes, as well as all other rock types.

The porphyry, granite, and breccia were impregnated with anhydrite veins and blebs during the potassic alteration and chalcopyrite-mineralizing phase. Meteoric fluids percolated down from the surface and hydrated the anhydrite, converting it to gypsum. This process, with the accompanying ~50% volume increase, shattered the host rock and filled the fractures with gypsum. Once the deposit was exposed by erosion, meteoric water filtered down and leached gypsum from the rock leaving weakly cemented or open fractures. The zone of poor rock quality migrated downward in the deposit area as a relatively flat hydration front. Below the hydration front, the mineralized rocks are less fractured and the anhydrite fracture filling is unaltered.

The Mirador porphyry system exhibits typical porphyry alteration zoning, with a core of potassic alteration evidenced by pervasive fine secondary biotite nuclei surrounded by a large (approximately 4 km²) quartz-sericite-pyrite (phyllic) alteration zone. The phyllic alteration weakly overprints much of the potassic alteration in the core of the system. Propylitic alteration is the most distal evidence of the porphyry.



10.0 EXPLORATION

The first exploration in the area of the Mirador deposit was conducted by Billiton. The area attracted Billiton's interest during the original reconnaissance geological and geochemical surveys completed in December 1994. These surveys, which included the collection of 315 stream sediment pan concentrate samples, identified a drainage area of roughly 50 sq km that contained anomalous grades of Cu, Mo, Au, Zn, and Ag. There was an exploration hiatus from 1995 to 1999, when the area of the present property was declared off limits by the Ecuadorian Government because of the border conflict between Ecuador and Perú.

After the peace treaty of July 1999, Billiton completed detailed follow-up surveys to better define the anomalous areas of the Mirador property. The company collected 746 soil samples along ridges and 219 rock chips from outcrops in stream drainages traversing the anomalous zones. This work, along with geological mapping, defined the main Mirador anomalous zone.

In April 2000, Billiton and Corriente entered into an agreement covering the area of the Mirador property.

Since April 2000, Corriente has carried out all of the exploration work on the Mirador property. The work completed has included geological mapping, pan concentrate sampling of stream sediments, soil geochemical sampling, rock chip sampling and the completion of 36,284 m of core drilling in 143 diamond drill holes at Mirador proper. The Mirador drill holes are consecutively numbered from M-1 to M-141, but there are two holes with the same collar number but designated differently with an "A" (M-74 and M-74A and M-139 and M-139A). As a result, in spite of the fact that the drill hole numbering sequence ends at M141, the total number of holes drilled to the end of 2005 is 143.

10.1 2000

In May 2000, the first phase of drilling at Mirador began, under the supervision of J. David Lowell, who was under contract to Corriente. A total of 5,383 m of drilling was completed in 30 core holes (M-1 to M-30).

10.2 2001

Between January and May of 2001, the second phase of drilling was carried out. Twenty-two core holes (M-31 to M-52) was completed, with an aggregate length of 8,136 m.

10.3 2002

The third phase of drilling was conducted between February and April of 2002, and 10 core holes (M-53 to M-62) were drilled, totalling 2,739 m. In October 2002, Corriente assumed the management of all aspects of the project.



10.4 2003

In February 2003 a Preliminary Assessment Report of the Mirador Deposit was completed and was filed as a Technical Report entitled "Mirador Project, Corriente Copper Belt, Southeast Ecuador, Order of Magnitude Study, Part 1, Technical Report". The Technical Report included a polygonal mineral resource estimate based on the 62 drill holes completed at Mirador between 2000 and 2002. Both the Technical Report and the mineral resource estimate were completed under the supervision of Qualified Persons James M. Dawson, P.Eng. and David K. Makepeace, P.Eng. (Dawson and Makepeace, 2003)

In July, Sumitomo of Japan completed independent metallurgy tests showing favourable concentrate potential. AMEC reviewed this work and found it to be done to industry standard, and subsequent follow-up work has confirmed its conclusions. Metallurgy is discussed in detail in Section 16 of this report.

10.5 2004

A fourth phase of drilling was conducted at Mirador between December 2003 and April 2004. A total of 8,091 m of core drilling was completed in 29 holes (M-63 to M-90, including M-74 and M-74A).

10.6 2005

Corriente conducted a fifth phase of drilling in 2005, and completed 11,935 m of core drilling in 52 holes (M91 to M141, including M139 and M139A). Much of this program involved the drilling of angled infill drill holes that were intended to better define the early porphyry dikes, which account for most of the lower-grade zones in the deposit. The data from the holes that intersected the dikes, together with new information from outcrops exposed during the construction of new drill trails, helped to confirm and refine contacts of known early porphyry dikes, particularly in the northern sector. A few holes targeted the late breccia dikes in the north part of the deposit, to better locate and define the contacts and to explore for potentially economic copper mineralization along the dike margins. The 2005 holes did not intersect any significant new dikes or any new areas of mineralization.

In addition to the drilling at Mirador, there was ongoing mapping of new drill trail exposures and remapping of outcrops exposed in stream channels. A six-kilometer pilot road was constructed to the east side of the deposit from the existing access road leading south from the camp. This created large new exposures of mostly weathered and leached rock. These exposures were geologically mapped, and the new data were added to the geological database. The new geological information required only minor changes to be made to the existing maps; two dikes proved to project farther east than previously interpreted. Re-mapping of outcrops in stream channels north and west of the deposit was completed, allowing more accurate control of contact locations and increased understanding of alteration styles there. A geotechnical-oriented re-mapping of fractures and other geologic structures was also completed late in 2005. Over 1200 measurements were collected in order to complement the oriented core structural data collected in the majority of the last 40 holes drilled. These data were submitted to Piteau Associates for incorporation into the geotechnical database for pit slope stability studies.



11.0 DRILLING

The Mirador deposit has been tested by 143 diamond drill holes totalling 36,284 m, arranged in a rough grid on approximately 75-m to 100-m centers. The drill hole information has been tabulated in Appendix B and the collar locations are shown in Figure 11.1.

Diamond drills belonging to the contractor Kluane International Drilling Inc. ("Kluane") of Canada were used to complete all the diamond-drilling programs. Kluane used a man-portable wire-line drill, and all platforms were accessed via hand-built trails. Until 2005, there was no road access to the drill pads and access was gained by walking 1,500 m along a trail from the road. Now, a rough access road leads into the east section of the drill area, and the drill platforms can be reached by short trails from the head of the road.

Drill core was recovered in standard NTW (5.7 cm) and BTW (4.2 cm) core tubes. The smaller BTW core was recovered from the lower parts of the deeper drill holes, after the rod string was changed to BTW diameter. Standard HQ size core (6.35 cm) was taken from a few of the geotechnical holes.

Because of the almost total lack of outcropping rock, very little was known of the geology of the Mirador deposit before the drilling campaigns began. Therefore, since the presence and orientation of any possible steeply dipping features could not be predicted, most of the early drill holes at Mirador were drilled vertically. As the geological knowledge of the deposit increased, it was recognized that there exist various geologic features with sub-vertical geometry, such as syn-mineral to post-mineral dikes and late-stage quartz-sulfide veinlets. Accordingly, in the 2004 and 2005 drilling programs, a greater percentage of holes with angles of -60° to -80° were drilled to help define such features. In spite of the presence of the high-angle geologic features, copper grades do not appear to be influenced by the angles of the holes.

Using a selected set of data, MDA compared grades, core recovery and Rock Quality Designation ("RQD") between angled and vertical holes. In order to compare "apples to apples", the samples selected were only from within the central mineralized breccia. This restricted the comparison to similar rock types and styles of mineralization and limited the comparison spatially. Working within these constraints, a fair comparison could be made of the grades in vertical and angled holes. Table 11.1 presents the results. It is interesting to note that in all cases the median grades are higher in the vertical holes, while the mean grades for all metals except zinc are higher for the vertical holes. As this did not appear to make sense geologically, and because the mean grade differences were positively correlated with the coefficients of variation (suggesting that the results might have been skewed by outliers), quantile plots were made comparing the distributions. There is a bias between angle and vertical holes:

- There is a minor change in distribution of copper;
- The mean and median gold grades are higher in vertical holes;

¹ A graphical technique for determining if two data sets come from populations with a common distribution or for determining population distributions.



- Silver has both a change in distribution and a bias in favor of vertical holes;
- Lead is biased in favor of vertical drilling in the less than 60-ppm range and for the lowest 80% of the population;
- There is a positive bias in favor of vertical holes for molybdenum; and
- Zinc has a change in distribution changing the relative amounts of high- and low-grade samples.

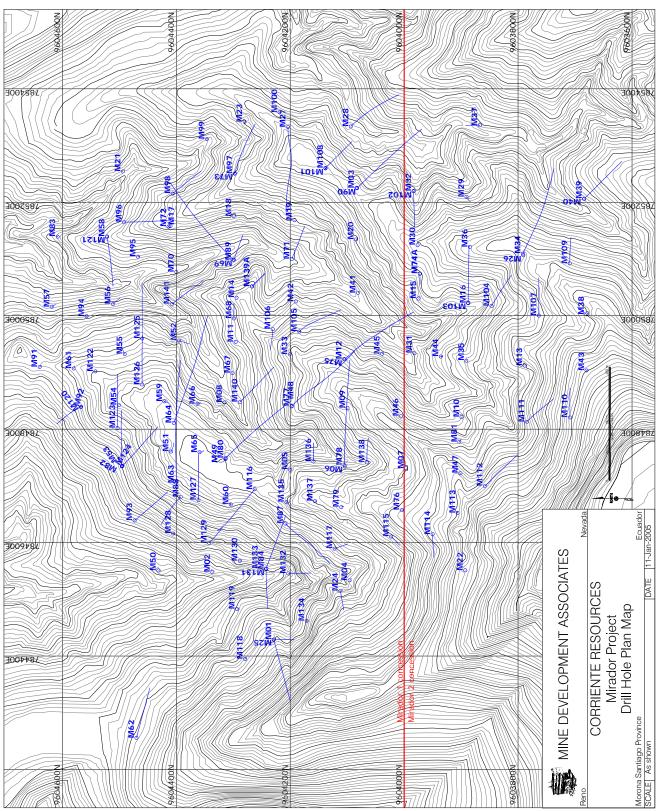
This analysis can continue and should continue to investigate fully the reason for these phenomena and their potential impact on grades used to estimate the resource. However, it can be said that there is a bias between angle and core holes in the central mineralized hydrothermal breccia, and the bias and grade distortions are different for each metal. This strongly suggests that the mineralization is multiphased, and that the different metals were deposited in different places at different times.

Table 11.1 Metal Grades by Vertical vs. Angle Hole

	Meters	Median	Mean	Std. Dev.	CV	Min.	Max.			
	Copper (%)									
Vertical	3219	0.60	0.56	0.28	0.50	0.03	1.79			
Difference	9%	9%	1%	-11%	-12%	50%	-29%			
Angle	2952	0.55	0.55	0.32	0.58	0.02	2.53			
All Groups	6171	0.58	0.56	0.30	0.54	0.02	2.53			
	Meters	Median		Std. Dev.	CV	Min.	Max.			
	Gold (g/t)									
Vertical	3219	0.16	0.18	0.17	0.94	0.02	3.16			
Difference	9%	13%	19%	48%	24%	67%	42%			
Angle	2952	0.14	0.15	0.12	0.76	0.01	2.23			
All Groups	6171	0.15	0.17	0.15	0.88	0.01	3.16			
	Meters	Median		Std. Dev.	CV	Min.	Max.			
			5	Silver (g/t)						
Vertical	1059	2.10	2.46	2.07	0.84	0.03	27.10			
Difference	59%	62%	36%	26%	-7%	-88%	163%			
Angle	664	1.30	1.81	1.64	0.90	0.25	10.30			
All Groups	1723	1.90	2.21	1.94	0.88	0.03	27.10			
	Meters	Median	Mean	Std. Dev.	CV	Min.	Max.			
				ead (ppm)						
Vertical	1059	19.00	69.55	404.57	5.82	4.00	6665.00			
Difference	59%	58%	69.55 77%	404.57 286%	119%	300%	594%			
Difference Angle	59% 664	58% 12.00	69.55 77% 39.39	404.57 286% 104.75	119% 2.66	300% 1.00	594% 960.00			
Difference	59% 664 1723	58% 12.00 16.00	69.55 77% 39.39 57.93	404.57 286% 104.75 324.04	119% 2.66 5.59	300% 1.00 1.00	594% 960.00 6665.00			
Difference Angle	59% 664	58% 12.00	69.55 77% 39.39 57.93 Mean	404.57 286% 104.75 324.04 Std. Dev.	119% 2.66 5.59	300% 1.00	594% 960.00			
Difference Angle All Groups	59% 664 1723 Meters	58% 12.00 16.00 Median	69.55 77% 39.39 57.93 Mean S	404.57 286% 104.75 324.04 Std. Dev.	119% 2.66 5.59 CV	300% 1.00 1.00 Min.	594% 960.00 6665.00 Max.			
Difference Angle All Groups Vertical	59% 664 1723 Meters 3219	58% 12.00 16.00 Median 32.00	69.55 77% 39.39 57.93 Mean Molyk 46.52	404.57 286% 104.75 324.04 Std. Dev. odenum (pp. 90.02	119% 2.66 5.59 CV m) 1.94	300% 1.00 1.00 Min. 4.00	594% 960.00 6665.00 Max. 2630.00			
Difference Angle All Groups Vertical Difference	59% 664 1723 Meters 3219 9%	58% 12.00 16.00 Median 32.00 7%	69.55 77% 39.39 57.93 Mean 3 Molyb 46.52 34%	404.57 286% 104.75 324.04 Std. Dev. odenum (pp. 90.02 224%	119% 2.66 5.59 CV m) 1.94 142%	300% 1.00 1.00 Min. 4.00 0%	594% 960.00 6665.00 Max. 2630.00 751%			
Difference Angle All Groups Vertical Difference Angle	59% 664 1723 Meters 3219 9% 2952	58% 12.00 16.00 Median 32.00 7% 30.00	69.55 77% 39.39 57.93 Mean 3 Molyk 46.52 34% 34.67	404.57 286% 104.75 324.04 Std. Dev. odenum (pp 90.02 224% 27.77	119% 2.66 5.59 CV m) 1.94 142% 0.80	300% 1.00 1.00 Min. 4.00 0% 4.00	594% 960.00 6665.00 Max. 2630.00 751% 309.00			
Difference Angle All Groups Vertical Difference	59% 664 1723 Meters 3219 9% 2952 6171	58% 12.00 16.00 Median 32.00 7% 30.00 30.00	69.55 77% 39.39 57.93 Mean 5 Molyk 46.52 34% 34.67 40.85	404.57 286% 104.75 324.04 Std. Dev. odenum (pp 90.02 224% 27.77 68.04	119% 2.66 5.59 CV m) 1.94 142% 0.80 1.67	300% 1.00 1.00 Min. 4.00 0% 4.00 4.00	594% 960.00 6665.00 Max. 2630.00 751% 309.00 2630.00			
Difference Angle All Groups Vertical Difference Angle	59% 664 1723 Meters 3219 9% 2952	58% 12.00 16.00 Median 32.00 7% 30.00	69.55 77% 39.39 57.93 Mean 9 Molyk 46.52 34% 34.67 40.85 Mean 9	404.57 286% 104.75 324.04 Std. Dev. odenum (pp. 90.02 224% 27.77 68.04 Std. Dev.	119% 2.66 5.59 CV m) 1.94 142% 0.80	300% 1.00 1.00 Min. 4.00 0% 4.00	594% 960.00 6665.00 Max. 2630.00 751% 309.00			
Difference Angle All Groups Vertical Difference Angle All Groups	59% 664 1723 Meters 3219 9% 2952 6171 Meters	58% 12.00 16.00 Median 32.00 7% 30.00 30.00 Median	69.55 77% 39.39 57.93 Mean 9 Molyk 46.52 34% 34.67 40.85 Mean 9	404.57 286% 104.75 324.04 Std. Dev. odenum (ppi 90.02 224% 27.77 68.04 Std. Dev.	119% 2.66 5.59 CV m) 1.94 142% 0.80 1.67	300% 1.00 1.00 Min. 4.00 0% 4.00 4.00 Min.	594% 960.00 6665.00 Max. 2630.00 751% 309.00 2630.00 Max.			
Difference Angle All Groups Vertical Difference Angle All Groups Vertical	59% 664 1723 Meters 3219 9% 2952 6171 Meters	58% 12.00 16.00 Median 32.00 7% 30.00 30.00 Median 46.00	69.55 77% 39.39 57.93 Mean 9 Molyk 46.52 34% 34.67 40.85 Mean 9	404.57 286% 104.75 324.04 Std. Dev. odenum (ppi 90.02 224% 27.77 68.04 Std. Dev. Linc (ppm) 310.31	119% 2.66 5.59 CV m) 1.94 142% 0.80 1.67 CV	300% 1.00 1.00 Min. 4.00 0% 4.00 4.00 Min.	594% 960.00 6665.00 Max. 2630.00 751% 309.00 2630.00 Max.			
Difference Angle All Groups Vertical Difference Angle All Groups Vertical Difference	59% 664 1723 Meters 3219 9% 2952 6171 Meters 2587 110%	58% 12.00 16.00 Median 32.00 7% 30.00 30.00 Median 46.00 23%	69.55 77% 39.39 57.93 Mean 9 46.52 34% 34.67 40.85 Mean 9 2	404.57 286% 104.75 324.04 Std. Dev. odenum (ppi 90.02 224% 27.77 68.04 Std. Dev. Cinc (ppm) 310.31 -51%	119% 2.66 5.59 CV m) 1.94 142% 0.80 1.67 CV 3.09 -18%	300% 1.00 1.00 Min. 4.00 0% 4.00 4.00 Min. 9.00 800%	594% 960.00 6665.00 Max. 2630.00 751% 309.00 2630.00 Max. 6255.00 -29%			
Difference Angle All Groups Vertical Difference Angle All Groups Vertical	59% 664 1723 Meters 3219 9% 2952 6171 Meters	58% 12.00 16.00 Median 32.00 7% 30.00 30.00 Median 46.00	69.55 77% 39.39 57.93 Mean 9 Molyk 46.52 34% 34.67 40.85 Mean 9	404.57 286% 104.75 324.04 Std. Dev. odenum (ppi 90.02 224% 27.77 68.04 Std. Dev. Linc (ppm) 310.31	119% 2.66 5.59 CV m) 1.94 142% 0.80 1.67 CV	300% 1.00 1.00 Min. 4.00 0% 4.00 4.00 Min.	594% 960.00 6665.00 Max. 2630.00 751% 309.00 2630.00 Max.			



Figure 11.1 Mirador Drill Hole Location Plan





The following field procedures were used in all of the Corriente drilling campaigns from 2001 to 2005:

- Core is stored in wooden boxes each holding five meters of core. When picked up at the drill, all
 the core box lids were secured and the boxes were packed out on foot by workers to the road,
 then loaded onto trucks and delivered to the Mirador camp. Corriente staff then opened the
 boxes and converted the drill hole depth markers from feet to meters. The core boxes were then
 placed on a stand and photographed in natural light.
- The core was marked at one-meter intervals by a geotechnician, who then measured the core recoveries and RQD. Technicians completed a preliminary drill log, wherein they recorded the core recovery, structural features, fracture density and orientation, and rock quality designation (RQD).
- The drill-hole collars were surveyed by Segundo Toledo Peláez of Topcon Survey S.A., using total station GPS brought in from differential GPS control points to reported instrument accuracy of ±1 m (X-Y) and ±2 m (Z). Some of these surveys were made before drilling, and so located only the excavated pads. The accuracy in these cases would be somewhat less than the accuracy of the equipment, approximately three meters.

Fifty of the one hundred and forty two drill holes had no down-hole surveys. Of the remainder, twenty holes in the second and third phases of drilling were surveyed using a Tropari instrument, and the holes drilled in 2004 and 2005 were surveyed using a Sperry-Sun instrument. Five of the unsurveyed drill holes were drilled at angles between -60° and -70° (M01, M25, M25, M39, and M62). These holes were drilled on the periphery of the deposit.

After the drill holes were completed, the collar locations were marked with a large PVC pipe capped with a plastic cover (Figure 11.2).







Core recovery is good for this type of deposit, and averages about 91% overall. Recovery exceeds 95% in the zones of hypogene mineralization, but relatively low core recovery is common in the leached rock near the surface. The RQD measurements indicate that the rock quality is very low through much of the deposit; the average of all RQD measurements is 38% (pers. comm., John Drobe, Corriente). Largely, the poor RQD is the result of the rock literally falling apart after the hydration of veinlet-hosted anhydrite to gypsum and the subsequent solution of the gypsum by groundwater.

For insight into geotechnical information with respect to rock type, the median, mean and CV (coefficient of variation or standard deviation / mean) are given in Figure 11.3 and Figure 11.4.

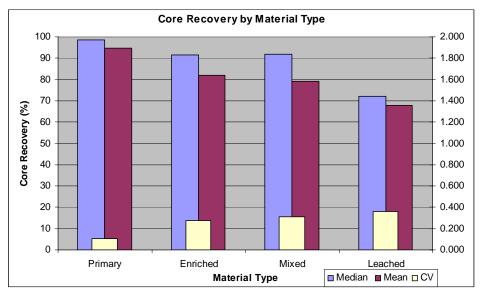


Figure 11.3 Core Recovery Statistics by Material Type

Note: median and mean are read on the left axis; CV on the right axis

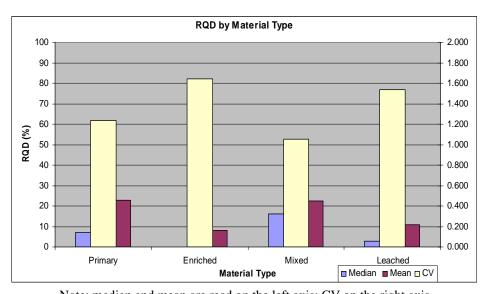


Figure 11.4 RQD Recovery Statistics by Material Type

Note: median and mean are read on the left axis; CV on the right axis

Specific gravity measurements were made on pieces of core that weighed from 10 grams to 30 grams each. The samples were collected at 40-m intervals. In the drill programs from 2000 to 2002, specific gravity was determined by the displacement method, where the sample was weighed dry, then immersed in water. The amount of water displaced by the sample was measured in order to determine its volume. The specific gravity was calculated by dividing the dry sample weight by the weight of the displaced water. This is not a very accurate method, since some water is lost because the sample always retains moisture, and it is difficult to measure accurately the volume of the displaced water. For the 2004



drilling program, the procedure was changed to the immersion method, where the samples were suspended with thin nylon monofilament and weighed dry, then immersed in water and weighed wet. This is generally a more accurate method, although porous samples must be sealed with a waterproof coating. There are 2,186 specific gravity measurements in the present (2006) database.



12.0 SAMPLING METHOD AND APPROACH

The drill core was delivered by truck to the Mirador camp. Corriente staff then opened the boxes and converted the drill hole depth markers from feet to meters. The core boxes were then placed on a stand and photographed in natural light.

The core was marked at one-meter intervals by a geotechnician, who then measured the core recoveries and RQD. Technicians completed a preliminary drill log, wherein they recorded the core recovery, structural features, fracture density and orientation, and RQD.

Each one-meter interval of core was assigned a sample number. Based on the style of mineralization, the individual one-meter samples were physically combined into composite samples of different lengths. The entire lengths of all the drill holes were sampled in this manner. The categories of mineralization used and the corresponding composite sample lengths were as follows:

- Leached zone (cap): five meters;
- Supergene copper-enriched zone: two meters;
- Hypogene (primary sulfide) zone: three meters; and
- Post-mineral dike: five meters.

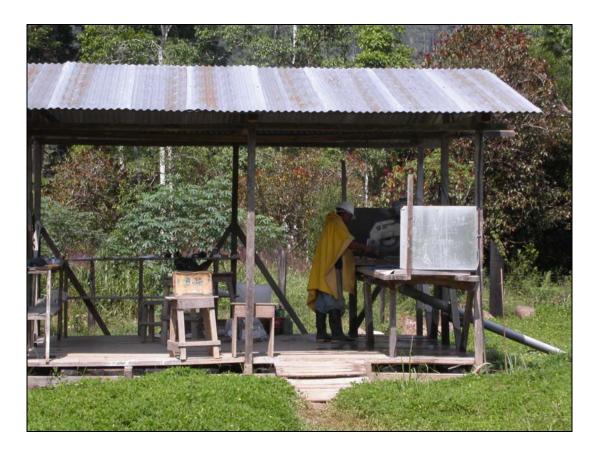
The use of non-random sample lengths in the database does introduce a certain degree of bias, but with compositing and length weighting the effect is minimized or eliminated. The standard practice is to use the same sample length for all material.

The sample intervals were recorded and assigned sample numbers. The core was split longitudinally using a diamond saw. No line was marked on the core to guide the splitting process. In cases where the core fragments were too small to be sawn, core fragments representing one-half of the core volume were randomly picked out of the core boxes by hand.

Each core sample was placed in its own plastic bag, and each bag was weighed and marked with the sample number. For the first four phases of drilling, the samples were sent to a preparation laboratory in Quito, Ecuador. During the fifth phase of drilling, Corriente used the Acme preparation laboratory in Cuenca, Ecuador. Upon arrival in Cuenca, the truck driver reported to the office manager at Corriente's offices. The truck then proceeded to the preparation laboratory, where the office manager prepared a list for the insertion of the duplicate and standard reference material (SRM) and QA/QC samples, and presented that list, and a sample shipment form, to the manager of the preparation facility. The lab manager confirmed the sample shipment and the work orders, and lab batch numbers were scanned and forwarded to Corriente via email. The sampling programs conducted between 2000 and 2005 were planned and executed in a satisfactory manner.



Figure 12.1 Core Saw Facility





13.0 SAMPLE PREPARATION, ANALYSES, AND SECURITY

13.1 Sample Preparation and Analyses 2000-2004

Sample pulps were prepared at ALS Chemex laboratories in Quito by laboratory personnel. Earlier samples were processed and analyzed by Bondar-Clegg prior to the merging of Bondar-Clegg and Chemex. Both of these preparation laboratories were independent from Corriente and its Ecuadorian subsidiary companies. Except for copper and gold, which were treated in a consistent manner, other elements that were analyzed varied somewhat through the period 2000 to 2004.

For all four drill phases from 2000 to 2004, the following procedures remained consistent. The whole sample was crushed to 75% passing –10 mesh, and then a one-kilogram sub-sample ("split") was pulverized to 95% passing –150 mesh. A 100 gram split ("pulp sample") was taken from the one-kilogram pulverized sample and shipped to the ALS Chemex laboratory in Vancouver, Canada. Here the pulp samples were fire assayed for gold with an atomic absorption finish (using a 30-gram aliquot), and were analyzed for copper and other elements using acid digestion/atomic absorption spectroscopy ("AAS") methods (AMEC 2004).

For the phase one and phase two drilling programs (2000 and 2001), the samples were assayed for gold using the fire assay technique with an AAS finish (FA-AAS), and analyzed for copper, silver, lead, molybdenum and zinc using four acid digestion followed by AAS.

Samples for the third drilling phase (2002) were assayed for gold using the FA-AAS technique and analyzed for copper, molybdenum and zinc using four acid digestion followed by AAS.

Samples for the fourth drilling phase (2004) were assayed for gold by FA-AAS and analyzed for copper and molybdenum using four acid digestion and AAS (AMEC 2004).

13.2 Sample Preparation and Analyses 2005

The 2005 drill core samples were prepared at the Acme Analytical Labs ("Acme") preparation facility in Cuenca, Ecuador. The sample preparation procedures were the same as were used in 2000 to 2004 by Bondar-Clegg and ALS Chemex, except that final sample pulverization was to 85% passing -200 mesh. The -200-mesh 100-g split material (pulp sample) was shipped to the Acme lab in Vancouver, Canada, for final analysis.

For the copper determination, one-half gram of material was digested using a four-acid solvent, followed by inductively coupled plasma/atomic emission spectrometric ("ICP-AES") analysis. Gold was determined by 30-gram fire-assay fusion followed by ICP-AES analysis. The sample preparation procedures are appropriate and well done, and the assays and analyses are of good quality.



13.3 Sample Security

In all five phases of drilling, drill core samples remained under the control of authorized Corriente personnel from the time they left the drill platforms until they were delivered to the preparation laboratory. For shipment, the individual sample bags were put into woven polypropylene bags. Each of these bags was marked with the project number, the drill-hole number and a number identifying its place in the sequence of bags in the sample shipment. The shipment bags were secured with tape and rope, and were sent to the preparation laboratory in a contracted vehicle. In 2005, the practice of marking the shipment bags with the drill hole number was discontinued, and shipment bags were secured by number-coded nylon "zip" ties before shipment.

In the opinion of MDA and Sivertz, the sample security measures taken by Corriente were satisfactory.



14.0 DATA VERIFICATION

14.1 Introduction

The following sections from 14.1 to 14.5 are taken *verbatim* from AMEC (2004) but there are formatting changes and the figure, table and appendix numbering is different. The present authors' comments or changes are placed in the body of AMEC's text in square brackets ([]) and are not italicized.

14.2 Definitions

Exploration Best Practices Guidelines and NI 43-101 regulations state that a program of data verification should accompany an exploration program to confirm validity of exploration data. Furthermore, the guidelines require that a quality assurance quality control (QAQC) program be in place. A QAQC program should include the insertion of various control sample types. The corresponding terms used in this report for the QAQC sample types are defined as follows:

<u>Twin samples</u> (TS; also referred to as "half-core samples or "core re-sampling"): are samples obtained by repeating the sampling in the proximity of the original location. In the case of core drilling, such samples are obtained by re-splitting the half-core samples, representing therefore ¼ of the core, or by taking the remaining half-core. These samples should be assayed by the same laboratory as the original samples, and are mainly used to assess the sampling variance.

<u>Coarse duplicates</u> (CD; also referred to as "coarse rejects" or "preparation duplicates"): are splits of sample rejects taken immediately after the first crushing and splitting step. These samples should be assayed by the same laboratory as the original samples, and provide information about the subsampling variance introduced during the preparation process.

<u>Coarse blanks</u> (CB): are coarse samples of barren material, which provide information about the possible contamination during preparation; the coarse blanks should be inserted into the sample sequence immediately after highly mineralized samples.

<u>Pulp duplicates</u> (PD; also called "same-pulp duplicates"): are second splits or resubmission of the prepared samples that are routinely analyzed by the primary laboratory. These samples are resubmitted to the same laboratory under a different sample number; these samples are indicators of the assay reproducibility or precision.

<u>Pulp blanks</u> (PB): are pulverized samples of barren material, which provide information about the possible contamination during assaying; these samples should be inserted into the sample sequence immediately after highly mineralized samples.

<u>Standard samples</u> (SS): are samples with well established grades, prepared under special conditions, usually by certified commercial laboratories. These samples are used to estimate the assay accuracy, together with the check samples.



<u>Twin, coarse and pulp check samples (TCS, CCS and PCS)</u>: are equivalents of the above defined twin samples, coarse and pulp duplicates, re-submitted in this case to an external certified laboratory (secondary laboratory). These samples are used to estimate the accuracy, together with the standards. Check sample batches should also include pulp duplicates of some of the samples included in the batch, as well as standard samples and pulp blanks, in reasonable proportions, in order to assess the precision, accuracy and possible assay contamination, respectively, at the secondary laboratory.

14.3 Quality Assurance/Quality Control (QA/QC) Programs 2000-2004

No QA/QC samples were inserted in the sample shipments for the Phase 1 drilling campaigns. Five percent of the samples from these drill programs were reanalysed with the benefit of SRM [Standard Reference Material] samples.

For Phase 2 drilling, the only QA/QC sample inserted into the sample shipments was a 100 g Lab Check Duplicate. This sample was taken on a 1 in 10 basis and was shipped to Chemex in Vancouver for analysis. The check lab was changed to Acme Labs in Vancouver after ALS Chemex purchased Bondar Clegg. No SRM samples were included in the shipment of any samples for these drill programs. The Lab Check Duplicate sample results were insufficient to certify the analysis results so a reassay program was set up by AMEC. Five percent of the samples from these drill programs were reanalysed with the benefit of SRM samples.

The sampling procedures were modified in February of 2001 to introduce some QA/QC samples into the sample shipments. The new protocol included inserting one pulp duplicate and one of three standards, GEM1, GEM2 and GEM3 into each batch of 20 samples sent to the labs. These standards were insufficiently homogenous to be used for a QA/QC program. This situation does not impact the quality of the grade values since 5% of the samples were reanalysed with the benefit of SRMs.

In late 2002, for the third phase of drilling, Corriente changed the insertion rate of the pulp duplicates and SRM samples to 1 in 40 samples. MS1 was the SRM sample being included in the lab shipments for this drilling campaign. The check samples were now being shipped to Acme labs in Vancouver but no SRM samples were being included in the shipments of the Lab Check Duplicate.

In late 2003, the sampling protocols were modified to include more QA/QC samples. During the 4th phase drilling program, the insertion rate of all QA/QC samples was increased back to a 1 in 20 insertion rate. The two SRMs included in the sample shipments were MS1 and MS2. A coarse reject duplicate was also included in the sample shipments. (A coarse split at -2 mesh was done only for samples destined for metallurgy test work and were only applied to drill holes M65 to M70.)

No blank samples were inserted into any of the sample shipments. Blank samples are used to certify sample preparation procedures by guarding against inter-sample contamination. They also are useful to identify sample mix-ups. It is recommended that Corriente include blank sample insertion in any future sampling programs.



With the inclusion of the reassay program and Corriente's current QA/QC protocols, the sample results are of sufficient quality to support a resource estimate.

14.3.1 ICP Sample Analysis

Three of the angled holes through the deposit, M75, M77and M80, were selected to check for any significant levels of potentially deleterious elements. 281 samples were analyzed for the following elements by ICP analysis; Au, Ag, Al, As, Ba, Be, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, Mg, Mn, Mo, Na, Ni, P, Pb, S, Sb, Sr, Ti, V, W, Zn and Hg. No elements reported ranges that would cause potential problems for the concentrate quality. This topic is discussed further in Section 16 of [the present] report.

14.3.2 Reassay of Phase 1 and 2 Drilling Samples

The drill core samples from Drill Phases 1, 2, and 3 were initially assayed without the benefit of adequate SRM samples. Phase 1 samples were sent to the assay lab with no SRM samples and Phase 2 and 3 samples were sent with an SRM that was insufficiently homogeneous. The pulps for 5% of the samples from these phases, 523 samples, were sent to ALS-Chemex under a blind sample-numbering scheme. Standards (MS1 and MS2) and pulp duplicates were inserted into batches of 20 samples.

The reassay data returned values for Cu and Au that are well within the accepted range to indicate that the original assays are of reasonable quality for resource estimation purposes. AMEC considers $\pm 10\%$ variation for 90% of the pulp duplicate analyses to demonstrate good precision. For the Cu grades, 90% of the population has an absolute relative difference of 11% whereas for the gold grades it was 18% (Figure 14-1 to 14-4). All SRMs submitted with these sample shipments returned values within the SRM accepted ranges. The Au grade differences are a little on the high side, probably due to the small subsample size of 100 g and the small aliquot size of 30 g.



Figure 14.1 QA/QC Reassay of Historical Data, Cu (ppm)

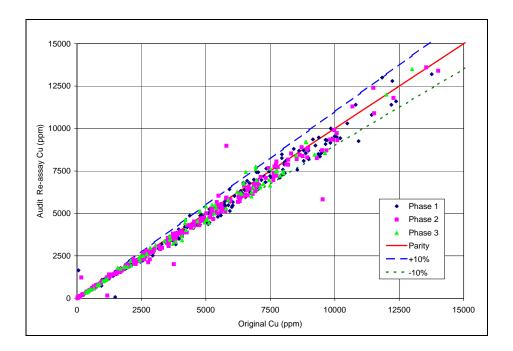


Figure 14.2 Reassay of Historical Data, Au (g/t)

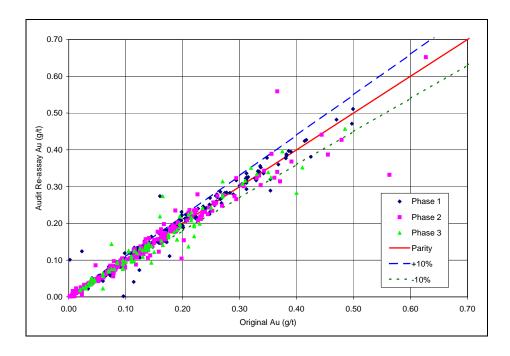




Figure 14.3 Percentile Rank Chart, Reassay Results, Cu (ppm), 501 Samples

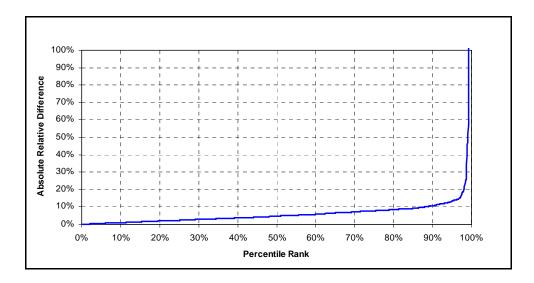
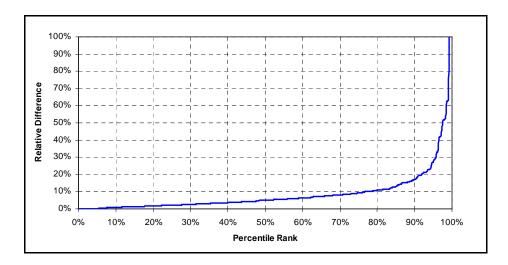


Figure 14.4 Percentile Rank Chart, Reassay Results, Au (g/t), 442 Samples



14.3.3 Standard Reference Material

In 2003, Corriente had the ALS prep lab in Quito prepare two new SRMs for them: MS1 and MS2. The procedures outlined below were used for making these SRMs.

The SRMs were prepared by extracting 100 kg of material from a homogenized 500 kg bulk sample of drill core rejects (-10 mesh). The material was pulverized in a standard laboratory rod mill by grinding the 100 kg of drill core rejects to -150 mesh and then blanket rolling them (four corners technique) to homogenize. The pulp was immediately stored in paper envelopes (100 g) ready for submission for round robin analysis.



MS1 represents the middle grade range for Cu and Au at the Mirador deposit (0.80 Cu % and 0.287 Au g/t) and MS2 is a low-grade Cu-Au standard (0.37 Cu % and 0.16 Au g/t). Both SRMs were submitted for round-robin analysis at four laboratories, Analytical Laboratories Ltd, ALS Chemex, International Plasma Laboratories (IPL) and Assayers Canada. Each laboratory received 10 samples. The round robin analysis results were of sufficiently good quality to establish the acceptance limits for the SRMs (See Figures 14-5 to 14-8). They were inserted into the sample shipments on a 2 in 40 basis.

If a SRM result was found to exceed twice the standard deviation value from the round robin study then the batch of 20 samples was reanalysed until the SRM returned an acceptable value. Some samples on the SRM charts are outside of the acceptable limits. These were not re-assayed as they were in areas outside of the mineralized envelope or in areas of below background grade range.

Figure 14.5 MS1 Round Robin and Sampling Results, Au (g/t), (DDH M63 to M90)

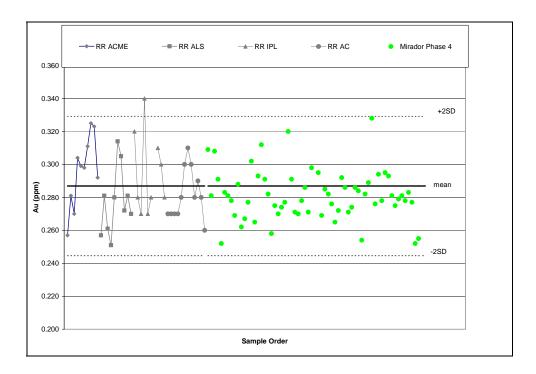




Figure 14.6 MS1 Round Robin and Sampling Results, Cu (%), (DDH M63 to M90)

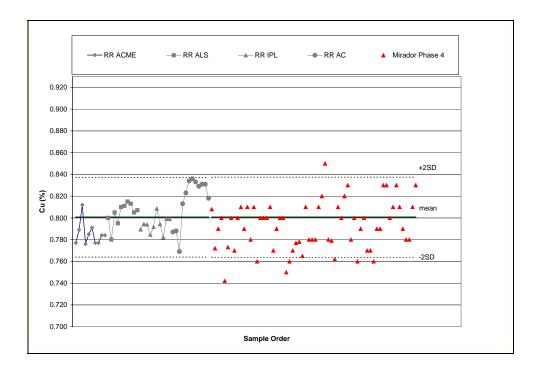
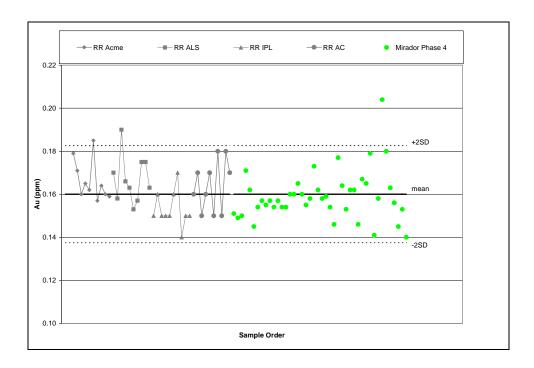


Figure 14.7 MS2 Round Robin and Sampling Results, Au (g/t), (DDH M72 to M90)





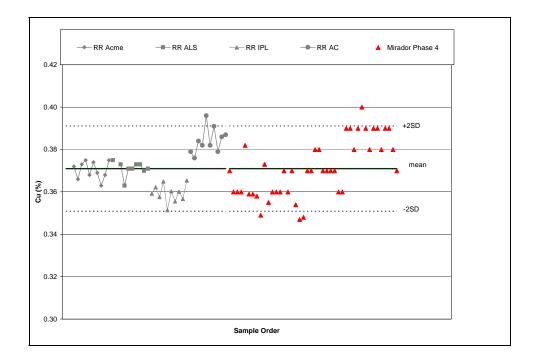


Figure 14.8 MS2 Round Robin and Sampling Results, Cu (%), (DDH M72 to M90)

14.3.4 Duplicate Samples

Four different types of duplicate samples were variably used at Mirador.

- 1. Phase 1 Only Lab Check Duplicates were taken during this phase of the drilling campaign on a 1 in 10 basis. AMEC has not reviewed the results from these samples. They have been superseded by the reassay results.
- 2. Phase 2 Pulp duplicates were included in the sample shipments on a 1 in 20 basis.
- 3. Phase 3 Pulp duplicates were included in the sample shipments on a 1 in 40 basis.
- 4. Phase 4 Pulp duplicates were included in the sample shipments on a 1 in 20 basis. Coarse Reject duplicates were introduced into the QA/QC program and were taken on a 1 in 20 basis. A small program was begun where for metallurgical holes, the samples were being crushed to ½" and a 1 to 2 kg sample was taken for metallurgical test work. For these holes, a duplicate was taken every 20 samples to monitor the performance of the assay results and study the impact of removing the subsample.

14.3.5 Coarse Crush Duplicates, ½" Crush Material

These duplicates were taken from drill holes M65 to M70 resulting in only 27 duplicate pairs. This is too small of a sample population for a detailed analysis but the few results that are present indicate no bias to the sample analysis results for Cu or Au (Figure 14-9 and 14-10).



14.3.6 Coarse Reject Duplicates

This duplicate type was only introduced during the 4th drilling campaign in 2003 to 2004. Corriente currently has 85 coarse reject duplicates in their database, representing coverage of 3.4% of total assayed samples.

The results of the coarse reject duplicate assays are shown in Figures 14-11 to 14-14. The performance of the Cu results is of excellent quality and reproduces well.

AMEC considers $\pm 20\%$ variation for 90% of the coarse reject duplicate analyses to demonstrate good precision. As seen in Figures 13-13 and 13-14, the variance for both the Cu and Au results are well below the accepted upper limit of 20%.

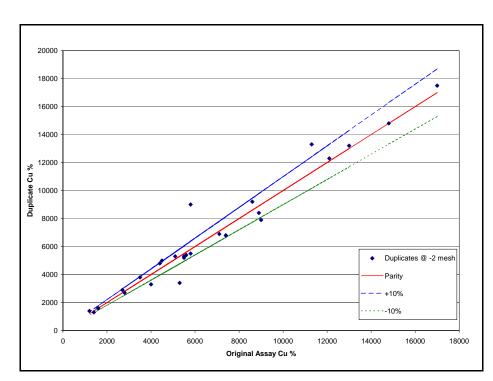
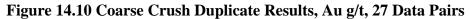


Figure 14.9 Coarse Crush Duplicate Results, Cu %, 27 Data Pairs





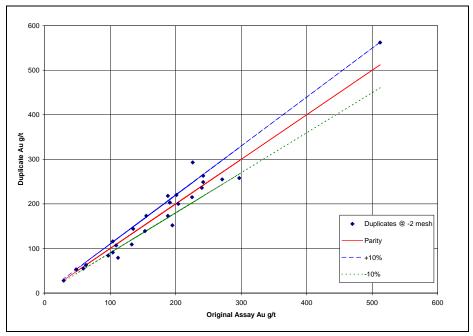


Figure 14.11 Coarse Reject Duplicate Results, Cu %, Scatter Plot

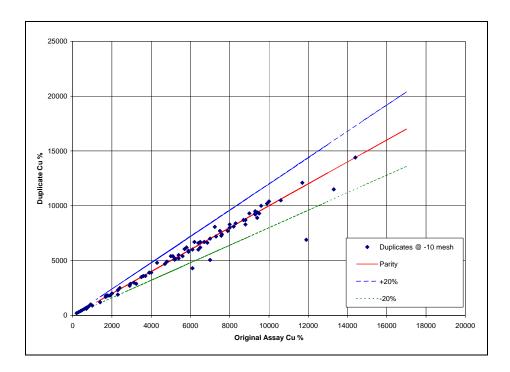




Figure 14.12 Coarse Reject Duplicate Results, Au g/t, Scatter Plot

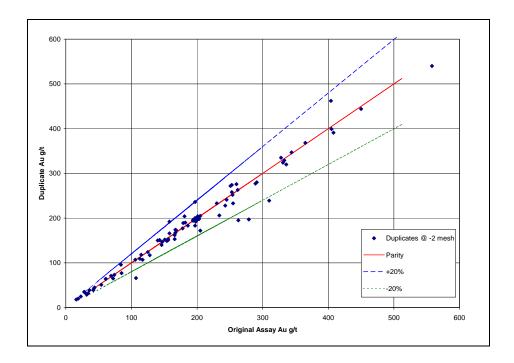
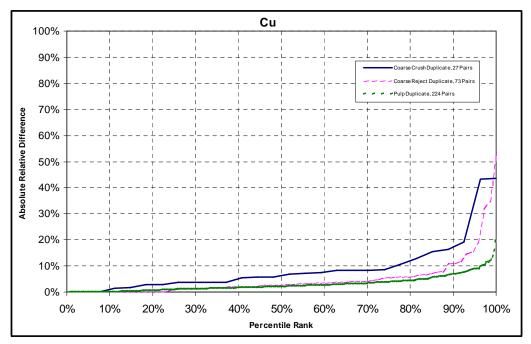


Figure 14.13 Duplicate Results, Cu %, Percentile Rank Chart





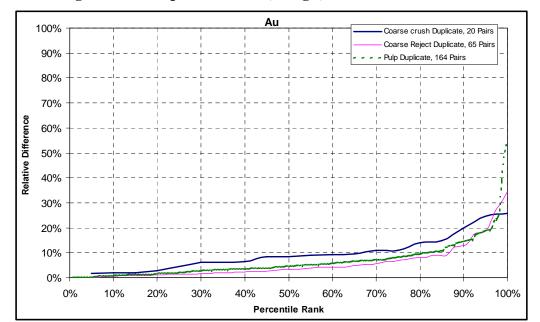


Figure 14.14 Duplicate Results, Au g/t, Percentile Rank Chart

14.3.7 Pulp Duplicates

There are 248 pulp duplicates in the Mirador database representing 4.3% of the assay database.

The results of the pulp duplicate assays are shown in Figures 14-13 and 14-16. Performance for the Cu values is excellent. The performance for the Au values is of acceptable quality considering its minor economic role in the deposit.

AMEC considers $\pm 10\%$ variation for 90% of the pulp duplicate analyses to demonstrate good precision. The Cu values are plotted in Figure 14-13 on a percentile rank chart. This chart shows that the Cu sample pairs are reporting 90% of the samples have a less than a 10% relative difference. The gold values however are reporting that 90% of the sample population has a relative difference of 15% (Figure 14-14); probably due to the small subsample size of 100 g and the small aliquot size of 30 g.



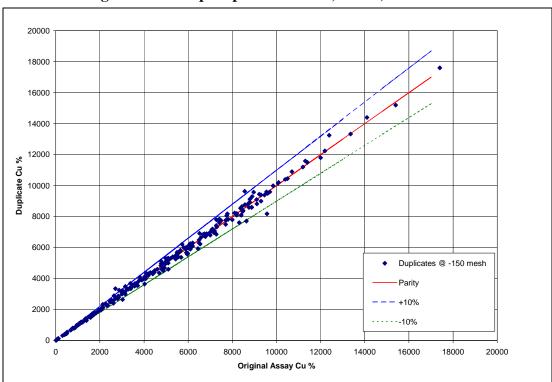
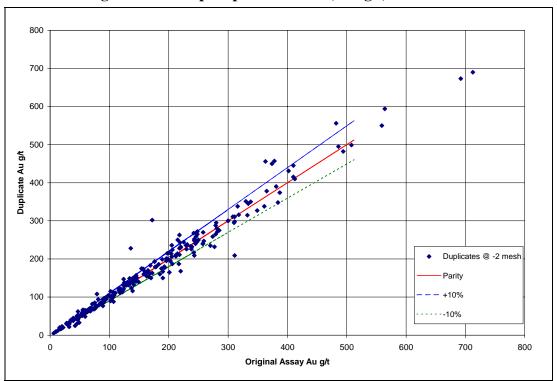


Figure 14.15 Pulp Duplicate Results, Cu %, Scatter Plot







14.3.8 Database Quality Control

AMEC completed a data quality check on 5% of the sample database used for the resource estimation. AMEC reviewed the collar surveys, downhole surveys, assay results and bulk density data and used original data sources to confirm the values in the database. The drill holes selected were M02, M12, M18, M33, M46, M54, M67, M77 and M87.

All the data was found to be of excellent quality and adequate for resource estimation purposes.

14.3.9 Assay Results and Lithology Codes

The assay results for 5% of the copper and gold were reconciled back to the original assay certificates issued by the assay laboratory. The sample intervals and sample number were confirmed by reconciliation to the drill logs for each of the drill holes. The lithology codes were confirmed using the drill logs. No errors were found during this review.

14.3.10 Downhole Surveys

AMEC checked all the survey disks for the downhole surveys during the site visit to the project. It was found that the geologists were not reading the down-hole tests correctly. On vertical holes, an incorrect azimuth was read on all holes. Corriente did not have a disk reader at the time but have since acquired one. All tests were reread using the proper instrument prior to completing the resource estimation.

During the phase 1 to 3 drill programs, two to three people read the survey disks and the results would be averaged. AMEC found many errors in the averaged value and some instances of errors in the readings. If the three readings are not in agreement than the results should be reviewed and the disks measured again until all are in agreement. Survey results should never be averaged.

14.3.11 Bulk Density

A total of 20 samples were sent to Teck-Cominco Labs in Vancouver for auditing; results agreed to within 3% for the first method and 0.6% for the second method (See [Table 14.1]). During the AMEC site visit, Corriente was advised that 5% of these samples should be validated at an independent laboratory.

Overall the averaged values differ very little between the original and the check result. The bulk density values are of sufficient quality for resource estimation purposes.



Table 14.1 Bulk Density Independent Check Results

Hole_ID	Date	Depth	Unit	Method	Corriente	TeckCominco	Relative %
		•					Difference
M16	2003	160	Jefp	1	2.67	2.56	-4.2
M44	2003	300	Jzgd	1	2.72	2.66	-2.2
M46	2003	280	Jzgd	1	2.78	2.54	-9.0
M48	2003	350	brmn	1	2.65	2.55	-3.8
M49	2003	400	Jzgd	1	2.75	2.69	-2.2
M51	2003	200	Jzgd	1	2.64	2.53	-4.3
M52	2003	220	Jzgd	1	2.62	2.59	-1.2
M55	2003	300	Jzgd	1	2.60	2.53	-2.7
M56	2003	340	Jzgd	1	2.63	2.66	1.1
				Avg:	2.67	2.59	-3.2
M63	2004	40.0		2	2.24	2.41	7.3
M63	2004	110.0		2	2.65	2.62	-1.1
M63	2004	170.0		2	2.85	2.83	-0.8
M64	2004	67.0		2	2.56	2.50	-2.3
M64	2004	290.0		2	2.72	2.69	-0.9
M64	2004	380.0		2	2.61	2.56	-1.9
M65	2004	140.0		2	2.53	2.48	-2.1
M65	2004	260.0		2	2.56	2.56	0.0
M66	2004	110.0		2	2.68	2.64	-1.6
M66	2004	140.0		2	2.57	2.52	-2.1
M66	2004	230.0		2	2.58	2.55	-1.3
				Avg:	2.60	2.58	-0.6

Methods: 1 = sample weighed dry, then immersed in water, and water displaced weighed; arm balance. 2 = suspended sample weighed in air, then immersed in water; electronic balance

14.4 Quality Assurance/Quality Control (QA/QC) Program 2005

14.4.1 Summary and Conclusions

The 2005 fifth phase drilling program included drill holes M91 through M141. The updated drill hole assay database contains 3,592 new assayed intervals from these holes. For the 2005 drilling program, Corriente generally followed the QA/QC guidelines recommended by AMEC Americas Ltd (AMEC 2004). MDA has reviewed the results of the 2005 Corriente QA/QC program but did not take independent samples from the 2005 drill holes. MDA did take independent samples from prior drilling campaigns.

The discussion in the following section relates to the 2005 program only.

The sample preparation procedures are appropriate and well done, and the assays and analyses are of good quality. Based on the results of the assays and analyses of standard samples inserted into the sample stream, there does not appear to be any significant bias in the assay or analytical data. The



results from the inserted blank samples indicate that the sample preparation procedures are conducted with appropriate care. Copper analyses of pulp duplicates reproduce well, while gold fire assays of pulp duplicates show modest variability. Although MDA does not believe that the modest variability in the reproducibility of gold assays has instilled any material bias or skewed the results, it is suggested that this phenomenon be investigated with a set of metallic screen samples. MDA and Sivertz also agree that a small percentage of samples should be sent "blind" to a second umpire laboratory, as a check on the primary laboratory.

14.4.2 Sample Preparation and Analysis

Samples for the 2005 (fifth phase) drilling were prepared and analyzed by the following procedure (paraphrased from John Drobe, 2005, personal communication):

The core was split by sawing or manual splitting and one-half of the core was used for sample analyses. The sampled intervals varied from 2 m to 5 m, depending upon the rock and style of mineralization, and so the samples typically weighed between 4 kg and 10 kg each. The samples were sent to the Acme sample preparation lab in Cuenca, Ecuador.

At the preparation lab, the samples were crushed to 70% passing 10 mesh. A split weighing one kilogram was taken from the crushed material for further processing, and the remainder was stored. As well, for every 1 in 20 samples, a second one-kilogram split was taken. This type of QA/QC sample is referred to as a "coarse-reject duplicate".

The minus 10-mesh one-kilogram split material was pulverized to 85% passing 200 mesh. A split weighing 100 g was taken from the pulverized material for assaying, and the rest was stored. In addition, for every one in 20 samples, a second 100-g split was taken. This type of QA/QC sample is referred to as a "pulp duplicate".

The coarse-reject duplicate material was inserted into the sample stream before pulverizing, and both the coarse-reject duplicate and pulp-duplicate samples were shipped with the regular samples. Approximately 2.5% of the final analyses (1 sample in 40) were of standard reference material (SRM) MS1, while another 2.5% were of SRM MS2. The purpose of this insertion procedure is to ensure that the duplicate and SRM samples are received "blind", that is, it is intended and expected that the analytical laboratory receiving the pulp samples will not be able to distinguish the SRMs and duplicates from the rest of the shipped pulp samples.

The minus 200-mesh (pulp) 100-g split material was shipped to Acme Analytical Laboratories Ltd ("Acme") in Vancouver, Canada, for final analysis. For the copper determinations, one-half gram of material was digested using a four-acid solvent, followed by inductively coupled plasma - atomic emission spectroscopy (ICP-AES) analysis. Gold was determined by 30-gram fire-assay fusion followed by ICP-AES analysis.

The rule followed by Corriente was that if a SRM sample returned a value in either copper or gold that was outside of an acceptable range, then Acme would be requested to reanalyze 10 samples on either side of the SRM, or halfway between the next SRM in the sample stream that



contained the questionable SRM result. The acceptable range was taken as the mean plus-orminus two standard deviations. Lomas (2004) discusses in detail the procedure for preparing the SRMs and the testing by which the SRM statistics were determined.

14.4.3 Duplicate Analyses on Pulps and Coarse Rejects

There are 183 copper and gold analytical results for duplicate-pulp samples, and 183 results for copper and gold on duplicate coarse-reject samples. These numbers represent about 5% of the total number of assay intervals in the Phase 5 (2005) drill hole database.

In general, there is good reproducibility for copper analyses between the original-sample grades and the duplicate-sample grades for both the pulp duplicates (Figure 14.17) and coarse-reject duplicates (Figure 14.19). The comparison between the original and the duplicate assays is not as good for gold as copper (Figure 14.18 and Figure 14.20; also note the R^2 statistic in Table 14.2). Statistics for the original sample and duplicate assays, and the R^2 value that measures the fit of the linear regression between the assay pairs are given in Table 14.2.



Figure 14.17 Copper Duplicate Assays – Pulps

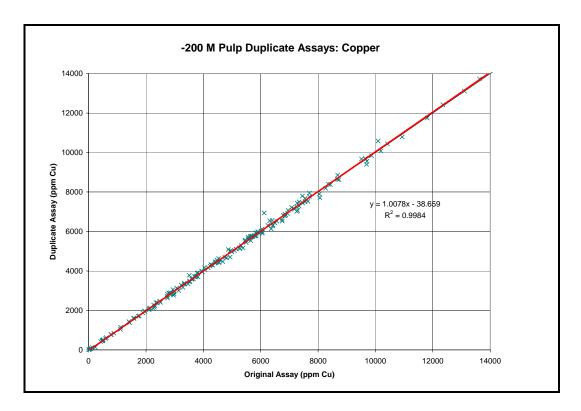


Figure 14.18 Gold Duplicate Assays – Pulps

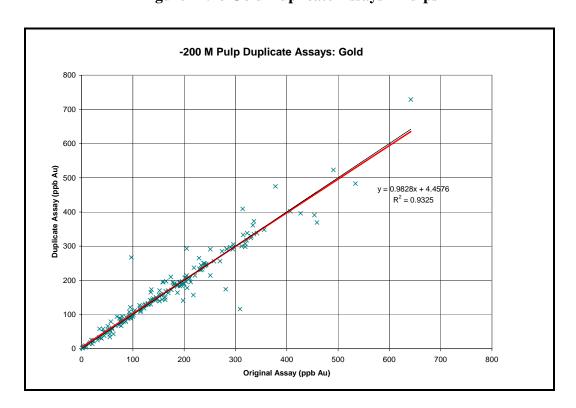




Figure 14.19 Copper Duplicate Assays – Coarse Rejects

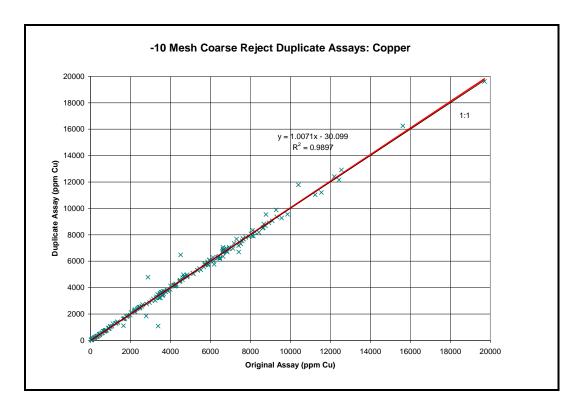
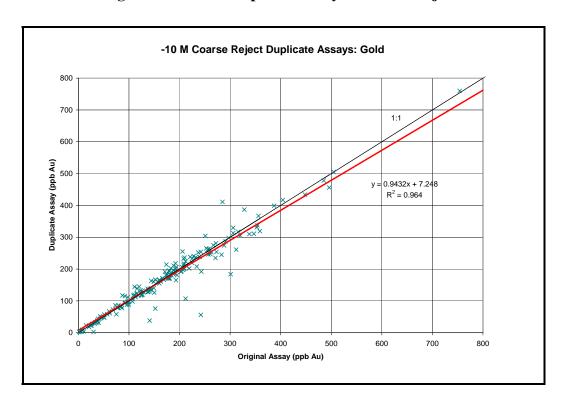


Figure 14.20 Gold Duplicate Assays – Coarse Rejects





Statistic	-200-mesh Pulp Originals	-200-mesh Pulp Duplicates	-10-mesh Coarse Reject Originals	-10-mesh Coarse Reject Duplicates
N Pairs	183		183	
Minimum Cu (ppm)	13	10	31	31
Maximum Cu (ppm)	23,444	23,957	19,706	19,620
Mean Cu (ppm)	4,901	4,900	4,575	4,577
Std Dev Cu (ppm)	3,142	3,169	3,269	3,309
R ² Cu	0.9984		0.9897	
Minimum Au (ppb)	1	2	2	2
Maximum Au (ppb)	642	729	1,567	1,433
Mean Au (ppb)	166	168	179	176
Std Dev Au (ppb)	112	114	151	145
R ² Au	0.9325		0.9640	

In Figures 14.21 through 14.24, the relative differences between the original assays and the duplicate assays are plotted in sorted-order according to the average grade of the sample pairs. At the low end of the grade distribution, reproducibility is relatively poor for both copper (below ~300 ppm) and gold (below ~ 100 ppb). Note that there is a low bias in the duplicate in the low end of the population, which is rather unusual since the same laboratory was used to analyze both the original and the duplicate samples. This bias occurs for both copper and gold, and for both pulps and coarse-rejects. The bias is not particularly significant, because its magnitude is less than the average variation between the assay pairs, and because it only occurs in the low-grade samples.

Figures 14.25 through 14.28 present the absolute value of the relative differences between assay pairs and their mean grade. This better illustrates the slight increase in reproducibility with increasing grade, even in the high-grade part of the distribution. These graphs quantify the analytical reproducibility of the duplicate samples.

Table 14.3 presents the statistics for samples with >=1000 ppm Cu and >=125 ppb Au, here defined as "significantly mineralized". Ninety percent of these significantly mineralized sample pairs have a relative difference in copper grades of up to 4% for pulps and up to 6% for the coarse rejects. The 90th percentile for gold is 23% for pulp duplicates and 21% for coarse-reject duplicates.



Table 14.3 Absolute Value of the Relative Difference between Sample Pairs

	-200-mesh Pulp Duplicates	-10-mesh Coarse Reject Duplicates
N Pairs for Cu>=1000 ppm	164	153
50 th percentile Cu	1%	2%
90 th percentile Cu	4%	6%
95 th percentile Cu	5%	9%
N Pairs for Au>=125 ppb	108	118
50 th percentile Au	4%	5%
90 th percentile Au	23%	21%
95 th percentile Au	39%	64%



Figure 14.21 Relative Differences of Copper Duplicate Assays – Pulps

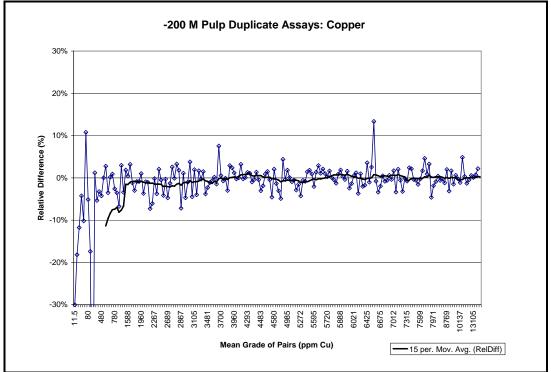


Figure 14.22 Relative Differences of Gold Duplicate Assays – Pulps

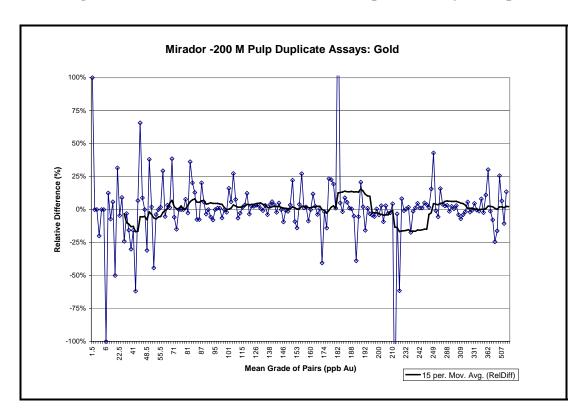




Figure 14.23 Relative Differences of Copper Duplicate Assays – Coarse Rejects

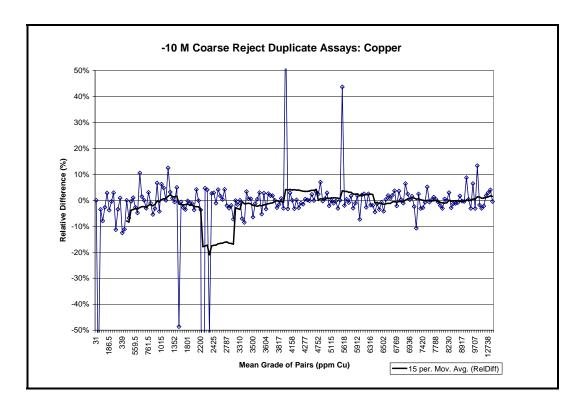


Figure 14.24 Relative Differences of Gold Duplicate Assays – Coarse Rejects

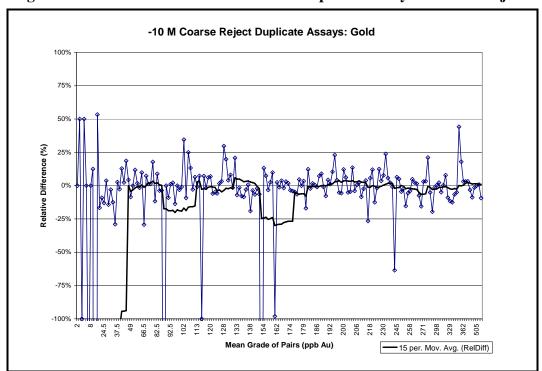




Figure 14.25 Absolute Value of the Relative Difference of Copper Duplicate Assays – Pulps

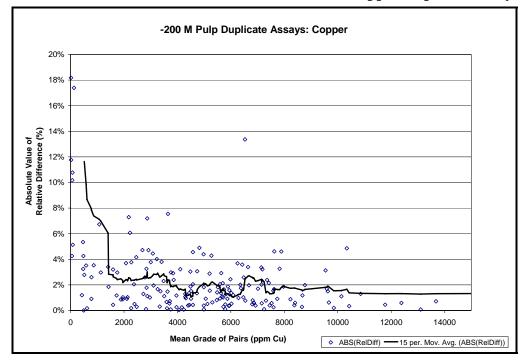


Figure 14.26 Absolute Value of the Relative Difference of Gold Duplicate Assays – Pulps

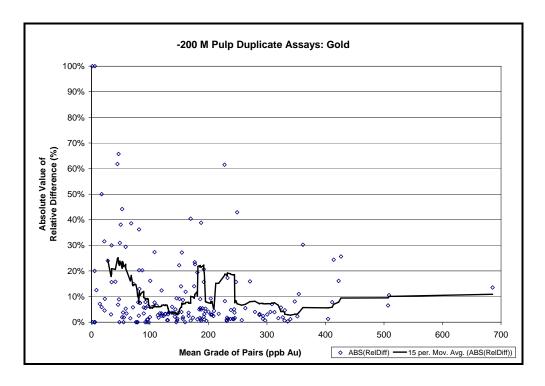




Figure 14.27 Absolute Value of the Relative Difference of Copper Duplicate Assays -Coarse Rejects

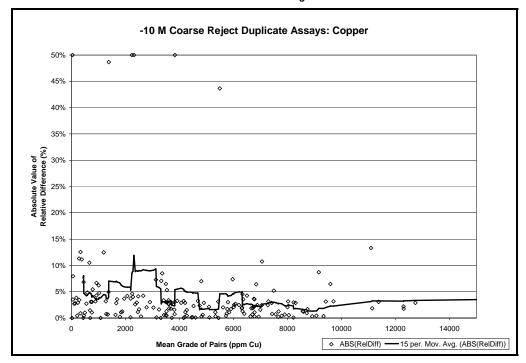
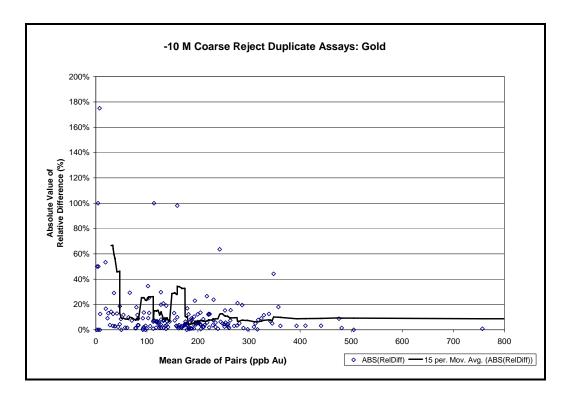


Figure 14.28 Absolute Value of the Relative Difference of Gold Duplicate Assays -Coarse Rejects





14.4.4 Standard Reference Samples

Standard Reference Material (SRM) samples were inserted into the stream of pulps sent to Acme in Vancouver. MS1 is of medium grade and MS2 is low grade. Ninety-three samples of MS1 and 88 samples of MS2 were analyzed, representing 2.6% and 2.4% of the total number of assay intervals in the Phase 5 drill hole database, respectively.

The assay results for MS1 and MS2 are shown in Figures 14.29 to 14.32. The samples are plotted by the order of the sample numbers. Those points marked as original assays were those that "failed" and were re-analyzed.

The first 15 analyses on MS1 appear to cluster on the low side for copper, but there is no corresponding cluster for gold. There is no biased clustering for copper or gold for the MS2 samples. The lab reanalyzed thirteen batches that were deemed to have failed because they returned grades more than approximately two standard deviations from the mean SRM grade. Seven batches with failed copper and gold values were not requested to be re-analyzed, although the gold content of the SRM itself was sometimes re-analyzed. Some batches that had a failed SRM assay were not re-tested, because the batch contained only samples from unmineralized or weakly mineralized drill holes located outside of the deposit (John Drobe, 2005, personal communication). Of the batches that were re-analyzed, 12 of the SRMs were high in copper, one was low in copper, one was high in gold, and three were low in gold. Two batches that were re-analyzed returned out-of-range SRM values for the second time as well. Table 14.4 lists the batch failures.

Table 14.4 List of Re-Analyzed Batches

	Batches Rerun		Batches Not Rerun	
	MS1	MS2	MS1	MS2
High Cu	5*	7	1	1
Low Cu	0	1	1	0
High Au	1	0	0	1
Low Au	1	2	1	2
# Batches	5	8	3	4
# Reruns w bad SRM	0	2	*	*

^{*}For one batch that was rerun, the high-Cu SRM was not rerun with the rest of the samples.



Figure 14.29 Standard MS1 Checks - Copper

Standard MS1 Analyses: Copper

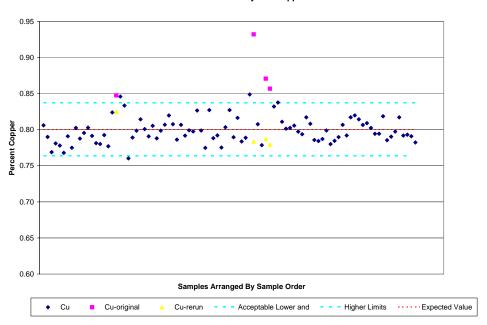


Figure 14.30 Standard MS1 Checks - Gold

Standard MS1 Analyses: Gold

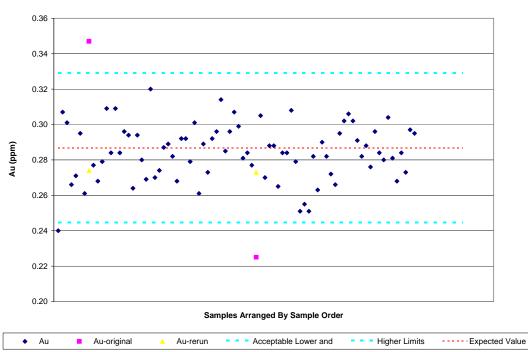




Figure 14.31 Standard MS2 Checks - Copper

Standard MS2 Analyses: Copper

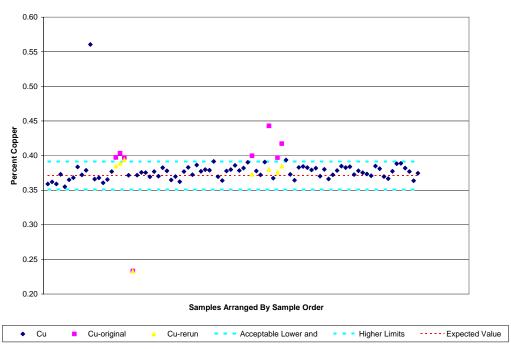
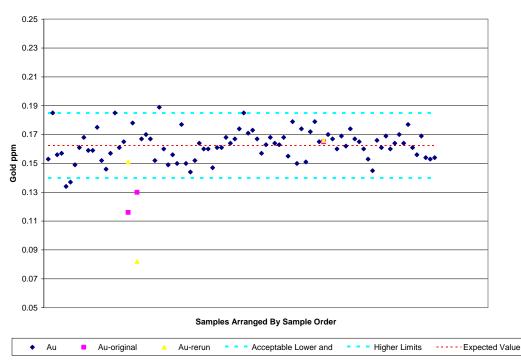


Figure 14.32 Standard MS2 Checks - Gold

Standard M2 Analyses: Gold





Descriptive statistics for the SRMs are given in Table 14.5. These statistics compare well with the parameters previously assigned to the SRMs, except that the copper for MS2 has some extreme outliers. Lomas (AMEC 2004) discusses the testing from which the SRM statistics were determined.

Table 14.5 Descriptive Statistics of the Standard Reference Material

	MS1		MS2
--	-----	--	-----

Phase 5	SRM	Phase 5	SRM
Analyses*	Determinations	Analyses*	Determinations
93	41	88	40
0.802	0.801	0.378	0.371
0.024	0.018	0.028	0.010
0.03	0.02	0.07	0.02
0.285	0.287	0.162	0.163
0.018	0.021	0.015	0.011
0.06	0.07	0.09	0.06
	93 0.802 0.024 0.03 0.285 0.018	Analyses* Determinations 93 41 0.802 0.801 0.024 0.018 0.03 0.02 0.285 0.287 0.018 0.021	Analyses* Determinations Analyses* 93 41 88 0.802 0.801 0.378 0.024 0.018 0.028 0.03 0.02 0.07 0.285 0.287 0.162 0.018 0.021 0.015

^{*} The statistics are based on first-run analyses and exclude the rerun analyses.

note: CV = std dev / mean



15.0 ADJACENT PROPERTIES

Other than the mineral prospects and exploration activities of Corriente itself, there are no known mineral deposits or advanced mineral exploration projects immediately adjacent to the Mirador property. Aurelian Resources Inc. ("Aurelian"), a publicly owned Canadian mineral exploration company, has acquired mineral concessions adjacent to the Mirador property. According to information posted on the Aurelian website, these are part of a large group of concessions that Aurelian has been exploring for precious and base metals (www.aurelian.ca).



16.0 MINERAL PROCESSING AND METALLURGICAL TESTING

16.1 Introduction

The original AMEC calculations were developed on 0.35% to 0.44% Cu cutoff to give a total in-pit resource of 110 million metric tonnes at an average grade of 0.67% Cu and 0.22 g/t Au. The majority of the feasibility metallurgical test work was done by the Lakefield and G&T labs mentioned below on four master composite samples. The test work resulted in an estimated copper recovery of 91% and a gold recovery of 47% based on a 29.8% Cu final copper concentrate grade with the gold reporting to the copper concentrate. The flow sheet developed to provide the metallurgical results was based on conventional copper-gold porphyry milling practices at typical grinds and with reagent types and rates.

Referencing chapter 18 of this document using a 0.37% Cu cutoff with an increased strip ratio, the resource base has been expanded to a total of 347 million metric tonnes at an average grade of 0.62% Cu and 0.20 g/mt Au. The hardness, recovery, and flotation concentrate grade of the expanded resource within the scope of the four master composite samples will be similar to the feasibility study metallurgical test work done in these regions. Drill holes outside the original scope of metallurgical test work have shown similar mineral and fracture characterization to the composite samples tested. Providing the copper-gold porphyry mineralization at depth is homogenous in nature, it is expected the hardness, recovery, and flotation concentrate grade found outside the original scope of metallurgical test work will continue to be consistent with the initial feasibility metallurgical results. Additional metallurgical test work should be completed to verify this last statement.

The following section is reproduced *verbatim* from the report titled "*Mirador Copper Project <u>Feasibility Study Report*"</u> dated May 2005 (AMEC Americas Limited, 2005). There are formatting changes and the figure, table and appendix numbering is different. The present authors' comments or changes are placed in the body of AMEC's text in square brackets ([]) and are not italicized.

16.2 History of Metallurgical Testwork

A significant amount of metallurgical testwork has been undertaken on mineralized samples from the Mirador deposit since 2001. SGS Lakefield Research (Lakefield), in Lakefield, Ontario, Canada, carried out the main program of feasibility testing between December 2003 and September 2004. The groups responsible historically for the metallurgical testing aspects of the project are summarized below:

- Geomet S.A., Santiago, Chile (May 2001)
 - o scoping batch rougher tests.
- Resource Development Inc. (RDI), Co, USA (May 2002)
 - o scoping batch rougher tests.



- Sumitomo Metal Mining Co, Limited, Japan (July 2003)
 - o scoping batch rougher and cleaner test,
 - o concentrate chemical and mineralogical analysis
 - o composite bond ball work index (BWI).
- SGS Lakefield Research Limited, Lakefield, Ontario, Canada (Dec 2003 Sept 2004)
 - o feasibility bench-scale flotation test program (batch and locked cycle flowsheet development and locked cycle variability testing)
 - o comminution testing (BWI, RWI, CWI, Ai and JK and SMC drop-weight testing) and modeling (JK SimMet)
 - QEM*SEM characterization of composite samples for variability testing
 - o concentrate characterization and dewatering.
- G&T Metallurgical Services Limited, Kamloops, BC, Canada (April Sept 2004)
 - o supporting bench-scale flotation testwork
 - o mineralogical modal analysis.
- MinnovEX Technologies Inc, Toronto, Ontario, Canada (July 2004)
 - o comminution testing (SPI) and modelling (CEET).

In 2001 Geomet S.A. conducted a scoping rougher flotation test, on behalf of Billiton Chile, on an unidentified sample (Muestra 2) from Mirador.

In April 2002, Resource Development Inc. (RDI) conducted three batch rougher flotation tests also on unidentified samples.

In June 2003, Sumitomo Metal Mining Co., Ltd. (Sumitomo) conducted an independent scoping level metallurgical program on five selected drill core samples. This testing included batch rougher and cleaner flotation, mineralogical and chemical analysis of concentrates, and a bond work index determination. The liberation characteristics of the ore were also investigated. AMEC reviewed this work and found it to be done to industry standard.

Overall, the results of the Geomet, RDI and Sumitomo testwork showed the samples tested had relatively simple metallurgy and favourable commercial concentration potential. The subsequent follow-up feasibility work by Lakefield on 3,000 kg of split diamond drill core from 18 drill holes across the ore body, and at various depths, has confirmed their conclusions.

The feasibility metallurgical testwork carried out by Lakefield was done under the direction of AMEC. Lakefield also provided samples to MinnovEX and G&T Metallurgical Services (G&T) to conduct SPI grindability testwork, and mineralogical and flotation quality control testwork respectively. Lakefield



and MinnovEX also conducted grinding circuit evaluations using their JKSimMet and Comminution Economic Evaluation Tool (CEET) simulation models respectively.

Lakefield's testing was conducted in two phases:

- Flowsheet Development December 2003 March 2004
 - o Mapping and Recovery Variability April September 2004.

Four master composites were produced from the core samples for an initial flowsheet and design criteria development program. This indicated the mill flow sheet for Mirador will be a conventional copper-gold porphyry flowsheet, with relatively coarse primary SAG and ball mill grinding to about 150 µm followed by copper rougher flotation, concentrate regrind to 30 µm, and cleaner flotation and dewatering. Metallurgical testing and mineralogical quantitative modal liberation analysis, conducted by G&T, supported the selection of the primary grind and regrind parameters.

A recovery and mineralogical variability mapping program completed during the third quarter of 2004 subsequently confirmed that the metallurgy and mineralogy of the ore body is quite simple and homogenous, and the samples tested responded consistently well to the conventional flowsheet and reagent scheme selected. Over 44 variability sub-composite samples were produced from 17 drillholes and tested by hole and depth. Each sample was subjected to chemical and QemSCAN (Quantitative Evaluation of Mineralogy by Scanning Electron Microscopy) mineralogical analysis, grindability testing, and locked cycle flotation. Locked cycle concentrates were subjected to mineralogical, chemical, pyroforicity, and dewatering testing.

Chemical analysis of the head samples indicated a range of copper grades from 0.20% to 1.07%, with average overall grade of 0.67%. Gold grades ranged from 0.05 g/t to 0.43 g/t with an average value of 0.22 g/t.

Concentrates produced are predicted to average 29.8% Cu at a recovery of 91%. The average gold grade and recovery was 5.2 g/t and 47.2%, respectively. A gold behaviour model developed from the flotation test data suggests gold tracks chalcopyrite, pyrite, and gangue, with near equal weighting throughout the process. There is good reconciliation between the test gold recovery data and that predicted by quantitative mineralogy.

A laboratory analysis of the individual locked cycle concentrate products indicated that no significant deleterious penalty element impurities were present and this is in good agreement with mineralogical mapping. Concentrate thickening and filtration testwork was conducted. The concentrates settled rapidly and no dewatering problems were identified. Pyroforicity results indicated the concentrate is not expected to be self-heating.

Grindability tests were conducted on the sub-composite intervals of core from individual drill holes. Two dedicated whole core geotechnical and comminution holes were also drilled and used for



additional grinding testwork, including Bond Work and Abrasion Indices, JK drop-weight and MinnovEX SPI testing.

Most of the ore in the pit falls geologically in an alteration zone of intense gypsum depletion. This is indicated by low RQD data and poor rock quality observed in drill core boxes. Comparative Bond low energy impact (CWI) and drop-weight test data also indicates the +150 mm ore lumps will break relatively easily at low-energy, but that the resulting reduction may be small. On this basis it is reasonable to assume the SAG mill feed granulometry will be relatively finer than the copper porphyry industry average.

JK and SPI testing data ranked the samples in the medium range of resistance to impact breakage for SAG milling. The ore exhibits low to moderate abrasivity. The average Bond ball mill work index is about 14.5 kWh/t and ranks the ore in hardness to ball milling as moderately soft relative to other copper porphyry ores in Lakefield's industry database and with relatively low variability. The JKTech drop weight and SPI test SAG mill parameters, and ball mill work indices, were used in JK SimMet and CEET simulation software models to confirm the grinding circuit design basis, and there was good agreement between both approaches.

16.3 Flowsheet

The estimated mineral resources included in the mine plan total approximately 111 Mt grading 0.67% Cu and 0.22 g/t Au. Silver and molybdenum are present but the grades are relatively low. Approximately 91 Mt of overlying waste rock will be removed over the mine life, resulting in an average strip ratio of 0.8:1. The process will be designed to treat 25,000 t/d of material.

A simplified schematic drawing of the proposed flowsheet is provided in Figure [16.1]. Run-of-mine open pit ore will be crushed in a gyratory crusher. The crushed ore will be processed by means of semi-autogenous and ball mill grinding followed by rougher flotation, regrind, cleaner flotation, and dewatering to produce copper concentrate. The concentrate will be trucked via the existing road network in the area to a port facility in Machala for shipment to smelters. Tailings from the process will be impounded in a tailings pond; water will be reclaimed from the tailings pond and reused in the process.



Crushing Rougher Flotation Primary Secondary Grinding Grinding Concentrate Regrind Cleaner/ 1st Cleaner Scavenger Tailings Management 2nd Cleaner Concentrate Concentrate Copper Thickening Dewatering Concentrate 3rd Cleaner

Figure 16.1 Simplified Mirador Flowsheet



17.0 MINERAL RESOURCE AND MINERAL RESERVE ESTIMATES

17.1 Introduction

Corriente requested that Mine Development Associates (MDA) complete a resource update on the Mirador Project. The incentive for the update was the inclusion of 52 new drill holes completed in 2005. This Phase 5 drilling program includes drill holes M91 through M141. The drill hole assay database contains 3,592 new assayed drill intervals for these holes.

The work done by MDA included a review of Corriente's geologic model and a QA/QC analysis, resource estimation, pit optimization, and pit design. MDA relied on previous work completed by AMEC, an independent mining and consulting group. In all cases, MDA attempted to utilize the same procedures unless compelling evidence suggested otherwise. The most important procedural changes were the definition of the lithologic, grade, and material-type zones, coding of the samples, and subblocking. Of less importance were the estimation parameters and the use of inverse distance to the fourth power instead of to the eighth power.

MDA's involvement with the Mirador project began in early 2005 with a site visit and a project review on behalf of a potential joint venture partner.

17.2 Corriente Geologic Model

A combination of material types, mineral domains, and lithologic codes (listed in Table 17.1 and illustrated in Figure 17.1 and Figure 17.2) were used to control grade estimation and assign density values. Material-type domains consist of the leached, mixed, and enriched zones in the weathered profile. For copper, mineral domains included grade shells and lithologic groups (pre-mineral dikes, post-mineral dikes, and post-mineral breccias) in the hypogene mineralization. Copper was modeled separately in each of the three weathered zone material types. Gold and silver were modeled identically to copper in the hypogene material using the same copper-grade shells and lithologic groups, but were modeled differently from copper in the weathered zones.

The rock unit "brmn" is the central breccia. While it is a distinct geologic unit, it has not been shown to have an effect on specific gravity, grades or metallurgy. Therefore, while it was modeled by solids, it was not used in any estimation and hence was not given a code.

In the hypogene material, the main grade shell, used for copper, gold, and silver, is defined by the change from grades dominantly above ~0.4% Cu to grades dominantly below ~0.4% Cu. This shell appears to be related to stockwork-dominated mineralization (above ~0.4% Cu), as opposed to disseminated-dominated mineralization (below ~0.4% Cu). A clear, albeit gradational (~0.2% Cu to ~0.6% Cu) separation is shown on quantile plots of the copper distribution (Attachment B). To compensate for the gradational changes in grade, two more shells were defined at ~0.2% Cu and ~0.6% Cu. These shells were defined manually (as opposed to using estimation, *i.e.*, using indicators, to account for local changes and variable drill hole and sample spacing).



Table 17.1 Coding and Description of the Geologic Model

Copper		
Code	Description	
1000	Hypogene "unmineralized": the material outside the mineralized shell (200)	
1200	Hypogene "mineralized": made up principally of disseminated and stockwork	
	mineralization inside a shell defined by ~0.4 %Cu	
1030	Early (pre-mineral) dikes (Jefp) which have similar though different styles of	
	mineralization to the enclosing 1000 and 1200	
1040	Late dikes (Jhbp) that post-date the mineralization but have incorporated some	
	mineralization during intrusion/stoping	
1050	Late breccias (brpm) that post-date the mineralization but have incorporated some	
	mineralization during intrusion/stoping	
2000	The enriched or supergene zone, which includes all lithologies	
3000	The mixed zone, which includes all lithologies	
4000	The leached zone, which includes all lithologies	
	Gold and Silver	
Code	Description	
30	These are early (pre-mineral) dikes (Jefp) which have similar but somewhat	
	different styles of mineralization to the enclosing 12340 and 12342	
40	These are late dikes (Jhbp) that post-date the mineralization but have incorporated	
	some mineralization during intrusion/stoping	
50	These are late breccias (brpm) post-date the mineralization but have incorporated	
	some mineralization during intrusion	
12340	All (external to the previous zones) "unmineralized": this is the material outside	
	the copper mineralized shell $(200)^2$ and the dikes and late breccias	
12342	All (external to the previous zones) "mineralized": this is made up principally of	
	disseminated and stockwork mineralization ³	

³ ditto

² A visual assessment suggests that this is an appropriate methodology and is consistent with the geology and mineralization of the deposit.



Figure 17.1 Schematic Illustration of Rock and Mineral Zones Used for Estimation - Copper

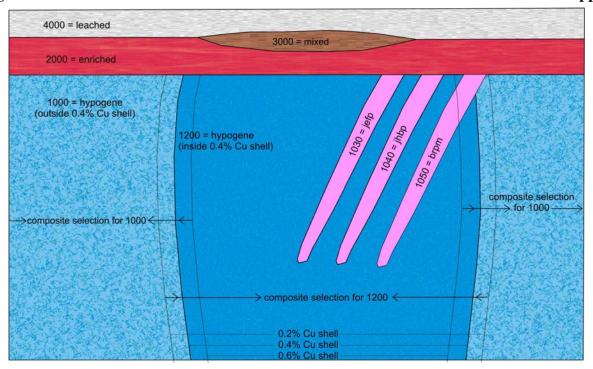
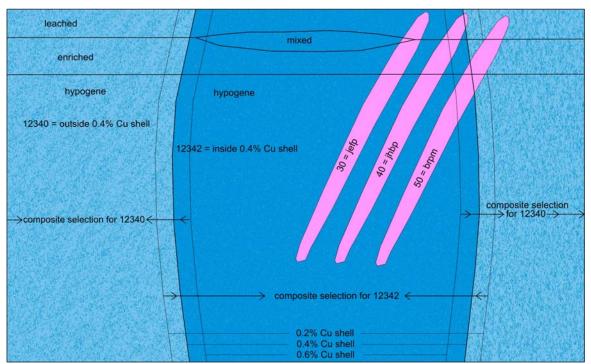


Figure 17.2 Schematic Illustration of Rock and Mineral Zones Used for Estimation –Gold and Silver





In the enriched, mixed, and leached zones, the copper has been remobilized and in general (at least apparently at the scale of the drilling) this leaching and remobilization did not affect the dikes and breccias. Gold seems to have maintained its original (pre-weathering) distribution. Silver distribution is most similar to gold distribution though a minor amount of remobilization does seem to have occurred.

The style of mineralization just described gave rise to the following modeling criteria. In the weathered zones near the surface, there are sharp geologic and grade contacts between the hypogene and enriched types, and between the enriched or mixed and leached material types. These contacts were modeled using lithologic and grade criteria. All lithologies (*i.e.*, dikes and breccias) in the enriched, mixed, and leached material types were treated for copper estimation as parts of each of the enriched, mixed or leached material types. In the hypogene rocks, each lithology (*i.e.*, country rock, dikes, and breccias) was estimated separately for copper. Gold and silver modeling honored all lithology types while ignoring material types.

Corriente constructed solids (30, 40, 50, 1000, 1200, 2000, 3000, and 4000) for the above-described units. While the weathering zones (1000, 2000, 3000, and 4000) were relatively simple and were used to clip each other to produce valid, non-overlapping solids, the porphyry dike and breccia solids (30, 40 and 50) were too complex for clipping because the solids overlap in too many ways. Therefore, a priority was assigned to these solids so that all coding was done in geologically chronological order (30 then 40 and then 50) for composite and block coding.

The previously described styles and interpretations of mineralization have statistical support, as there is sufficiently good correlation (statistically) between hypogene precious metal and copper mineralization to utilize the same shells for both.

17.3 Sample Coding and Compositing

Two grade shells (\sim 0.2% Cu and \sim 0.6% Cu) were used to code samples, while only one shell (\sim 0.4% Cu) was used for controlling the estimation and model block coding. Those samples lying outside the 0.6% Cu shell were used to estimate blocks outside the 0.4% Cu shell while those samples lying inside the 0.2% Cu shell were used to estimate grades inside the 0.4% Cu shell. Table 17.1 provides a schematic illustration of this. By coding and using samples in this manner, gradational changes were instilled in the model around the 0.4% Cu grade shell.

Overall, the deposit mineralization is evenly distributed and requires little capping or grade-projection constraints for the estimation process. Sample descriptive statistics were calculated for copper, gold, and silver for each of the modeled units and are presented in Attachment C.

Compositing was done to six meters (one-half of the final block size) honoring all material type, grade shell, and lithologic contacts after capping. The volume inside the main hypogene mineralization (~0.4% Cu shell) was estimated using composites from inside the 0.2% Cu shell. The volume outside

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⁴ As the silver does not make a major contribution to the economics of the deposit and the remobilization is small enough, the lack of specific attention to remobilization during modeling is likely not an important omission.. There does, however, seem to be a slight enrichment of silver in the enriched zone and the users of the model should be cognizant of this.



the main hypogene mineralization (outside the ~0.4% Cu shell) was estimated using all composites from outside the 0.6% Cu shell.

17.4 Specific Gravity Model

MDA assessed the specific gravity (SG) data in context of the defined lithologic and material types. Unless compelling reasons were found to change the methodology, MDA used the same methodology as in past estimates. MDA did have a different database and as a result, the mean specific gravity values of the various lithologies and material types were different from before. MDA decreased the measured mean specific gravity by 2% to account for the unavoidable sample selection bias⁵ introduced when choosing samples for density measurements. Table 17.2 presents the specific gravity values used in this resource estimate.

Zone/Lith	No. Samples	SG*	SG***
1000&1200	962	2.63**	2.58**
1030	142	2.65	2.60
1040	121	2 63	2.58

Table 17.2 List of Specific Gravity Values Used in Model

17.5 Resource Model and Estimation

The dikes and breccias are barren to weakly or erratically mineralized, and so are distinctly different from the main mineralization. The geological conditions in the deposit are probably much more complex than the interpretation that is presented in this model, in spite of Corriente's valiant efforts to accurately model pre- and post-mineral dikes and breccias. There are likely slightly fewer tonnes and slightly higher grade in the resource than is estimated, but at the scale of mining this may or may not be noticeable.

The block model was constructed with sub-blocks measuring 3.75 m by 3.75 m by 3 m (high). After estimation, the sub-blocks were re-blocked into blocks 15 m by 15 m by 12 m high; this is the same block size as the 2004 AMEC model. The model sub-blocked only when the contacts transected blocks. This procedure of re-blocking allows for better representation of the rapid grade changes across the pre-and post-mineral dikes and breccias and allows for local dilution at and across the contacts. If mining could execute effective grade control at block sizes of less than 15 m, then re-blocking the model to blocks smaller than 15 m by 15 m by 12 m (high) would be appropriate.

¹⁰⁴⁰ 1050 103 2.61 2.56 2000 2.52 2.47 109 3000 75 2.46 2.41 2.33 4000 154 2.38

^{*} before the 2% reduction;

^{**} estimated into each block by inverse distance

^{***} post-2% reduction

⁵ When sampling for specific gravity testing, one can only test material that is intact, and not material that is broken, fractured, brecciated, *etc*. This type of material has lower specific gravity.



Historic work by AMEC in 2004 emphasized geostatistics. MDA relied on AMEC's geostatistical results if nothing contradictory was found, but MDA still performed geostatistics to assess the applicability of the historic estimation parameters. Variograms were calculated for all zones, but only those with sufficient samples, which include the main mineralized zone and the surrounding low grade, could be modeled. The lack of sufficient samples, compounded by the fact that there might be poorer grade continuity, prevented the development of good variogram structures in the enriched, mixed, leached material types and in the post-mineral dikes and breccias. The variograms were used to support the chosen search ranges used in estimation.

Both the 2004 AMEC estimate and this estimate used inverse distance estimation for the final and reported estimate. Since the variograms did support the ranges used in the previous estimate, and since it was desirable to maintain consistency, MDA used similar search ranges. During this study, it was found that while copper does display some anisotropy (400 m in a northeast direction and 200 m in the northwest direction), gold and silver grade distribution is isotropic.

MDA estimated numerous models to assess the impacts of:

- the new grade shell and lithologic solids,
- the varying estimation parameters, and
- the 2005 drilling.

MDA estimated two models for each of those listed above; one used inverse-distance squared and one used the nearest-neighbor method. Modifications were made to the final estimate based on the results and comparisons of each of the interim models. No Kriging was done, as most zones did not produce variogram structures that could be modeled. The estimation parameters used in the final estimate are given in Table 17.3, Table 17.4, and Table 17.5.

MDA initially used an inverse distance power of three (ID³) and noted a rather steep relative drop in the amount of material grading over 0.7% Cu compared to the previous estimate, which used the power of eight in inverse distance estimation. This latter high power has a tendency to eliminate smoothing, approaching a nearest neighbor or polygonal estimate. Because this deposit has few high-grade outliers and is a relatively well-behaved deposit with respect to grade continuity, MDA felt that a lower power would be more appropriate. Due to a desire to maintain a certain amount of continuity in estimation techniques, MDA assessed the differences in estimation parameters⁶. The model was run at inverse powers of 3, 4, and 8 to study the sensitivities to heavily localizing the estimation. Based on the results of comparisons of these other models and on point validation studies, there was no compelling reason to choose ID³ over ID⁴. Therefore, ID⁴ methodology was chosen to maintain a certain amount of consistency with previous estimates, while also aiming to move away from a polygonal type of estimate. Examples of the copper and gold grade models are given in Figure 17.3 and Figure 17.4, respectively.

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⁶ Search distance, inverse distance power, number of samples, minimum number of samples, and maximum number of samples per hole.



Table 17.3 Estimation Parameters for Copper by Mineral Domain

Description	Parameter		
Main Hypogene Mineralization – disseminated low-grade (12340) Copper			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor	200 / 200 / 200		
Inverse distance power	4		
High-grade restrictions	None		
Main Hypogene Mineralization – disseminated and stockwor	k (12342): Copper		
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 200		
Inverse distance power	4		
High-grade restrictions	None		
Enriched Mineralization – (2000) Copper			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 50		
Inverse distance power	4		
High-grade restrictions	None		
Mixed Mineralization – (3000) Copper			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 50		
Inverse distance power	4		
High-grade restrictions (grade in Cu% and distance in m)	None		
Leached Zone – (4000) Copper – Pass 1	•		
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 50		
Inverse distance power	4		
High-grade restrictions (grade in Cu% and distance in m)	Only comps <=0.2% Cu		
Leached Zone – (4000) Copper – Pass 2			
Samples: minimum/maximum/maximum per hole	2/14/5		
Rotation/Dip/Tilt (searches)	140° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	20 / 20 / 20		
Inverse distance power	4		
High-grade restrictions (grade in Cu% and distance in m)	None		



Table 17.3 Estimation Parameters for Copper by Mineral Domain (continued)

Description	Parameter			
Pre-Mineral Porphyry – disseminated and stockwork (30, Jefp): Copper				
Samples: minimum/maximum/maximum per hole	1 / 14 / 4			
Rotation/Dip/Tilt (searches)	110° / -90° / 0°			
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 100			
Inverse distance power	4			
High-grade restrictions (grade in Cu% and distance in m)	None			
Post-Mineral Porphyry (40, Jhbp): Copper – Pa	ass 1			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4			
Rotation/Dip/Tilt (searches)	140° / -90° / 0°			
Search (m): major/semimajor/minor (vertical)	200 / 200 / 100			
Inverse distance power	4			
High-grade restrictions (grade in Cu% and distance in m)	Only comps <=0.1% Cu			
Post-Mineral Porphyry (40, Jhbp): Copper – Pa	ass 2			
Samples: minimum/maximum/maximum per hole	2/14/5			
Rotation/Dip/Tilt (searches)	140° / -90° / 0°			
Search (m): major/semimajor/minor (vertical)	20 / 20 / 20			
Inverse distance power	4			
High-grade restrictions (grade in Cu% and distance in m)	None			
Post-Mineral Breccia (50, brpm): Copper – Pa	ss 1			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4			
Rotation/Dip/Tilt (searches)	130° / -90° / 0°			
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 100			
Inverse distance power	4			
High-grade restrictions (grade in Cu% and distance in m)	Only comps <=0.1% Cu			
Post-Mineral Breccia (50, brpm): Copper – Pass 2				
Samples: minimum/maximum/maximum per hole	2/14/5			
Rotation/Dip/Tilt (searches)	130° / -90° / 0°			
Search (m): major/semimajor/minor ("vertical")	20 / 20 / 20			
Inverse distance power	4			
High-grade restrictions (grade in Cu% and distance in m)	None			



Table 17.4 Estimation Parameters for Gold by Mineral Domain

Main Hypogene Mineralization – disseminated low-grade (12340) Gold			
Samples: minimum/maximum/maximum per hole	1/14/4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor	200 / 200 / 200		
Inverse distance power	4		
High-grade restrictions	None		
Main Hypogene Mineralization – disseminated and stockwo			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 200		
Inverse distance power	4		
	·		
High-grade restrictions	None		
Pre-Mineral Porphyry – disseminated and stockwork (3			
Samples: minimum/maximum per hole	1/14/4		
Rotation/Dip/Tilt (searches)	110° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 100		
Inverse distance power	4		
High-grade restrictions (grade in ppb Au and distance in m)	None		
Post-Mineral Porphyry (40, Jhbp): Gold – Pa			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	140° / -90° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 100		
Inverse distance power	4		
High-grade restrictions (grade in ppb Au and distance in m)	Only comps <=40 ppb Au		
Post-Mineral Porphyry (40, Jhbp): Gold – Pa	ass 2		
Samples: minimum/maximum/maximum per hole	2 / 14 / 5		
Rotation/Dip/Tilt (searches)	140° / -90° / 0°		
Search (m): major/semimajor/minor (vertical)	20 / 20 / 20		
Inverse distance power	4		
High-grade restrictions (grade in ppb Au and distance in m)	None		
Post-Mineral Breccia (50, brpm): Gold – Pass 1			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	130° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 100		
Inverse distance power	4		
High-grade restrictions (grade in Cu% and distance in m)	Only comps <=40 ppb Au		
Post-Mineral Breccia (50, brpm): Gold – Pass 2			
Samples: minimum/maximum/maximum per hole	2 / 14 / 5		
Rotation/Dip/Tilt (searches)	130° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	20 / 20 / 20		
Inverse distance power	4		



Table 17.5 Estimation Parameters for Silver by Mineral Domain

Main Hypogene Mineralization – disseminated low-grade (12340) Silver			
Samples: minimum/maximum/maximum per hole	1/14/4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor	200 / 200 / 200		
Inverse distance power	4		
High-grade restrictions	None		
Main Hypogene Mineralization – disseminated and stockwol			
Samples: minimum/maximum/maximum per hole	1/14/4		
Rotation/Dip/Tilt (searches)	0° / 0° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 200		
Inverse distance power	4		
High-grade restrictions	None		
Pre-Mineral Porphyry – disseminated and stockwork (30 Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	1/14/4 $110^{\circ}/-90^{\circ}/0^{\circ}$		
1 , , , , ,	200 / 200 / 100		
Search (m): major/semimajor/minor ("vertical")			
Inverse distance power	4		
High-grade restrictions (grade in ppm Ag and distance in m)	None		
Post-Mineral Porphyry (40, Jhbp): Silver – Pa			
Samples: minimum/maximum per hole	1/14/4		
Rotation/Dip/Tilt (searches)	140° / -90° / 0°		
Search (m): major/semimajor/minor (vertical)	200 / 200 / 100		
Inverse distance power	4		
High-grade restrictions (grade in ppm Ag and distance in m)	Only comps <=0.4 ppm Ag		
Post-Mineral Breccia (40, Jhbp): Silver – Pas			
Samples: minimum/maximum per hole	2/14/5		
Rotation/Dip/Tilt (searches)	140° / -90° / 0°		
Search (m): major/semimajor/minor (vertical)	20 / 20 / 20		
Inverse distance power	4		
High-grade restrictions (grade in ppm Ag and distance in m)	None		
Post-Mineral Breccia (50, brpm): Silver – Pass 1			
Samples: minimum/maximum/maximum per hole	1 / 14 / 4		
Rotation/Dip/Tilt (searches)	130° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	200 / 200 / 100		
Inverse distance power	4		
High-grade restrictions (grade in ppm Ag and distance in m)	Only comps <=0.4 ppm Ag		
Post-Mineral Porphyry (50, brpm): Silver – Pass 2			
Samples: minimum/maximum/maximum per hole	2/14/5		
Rotation/Dip/Tilt (searches)	130° / -90° / 0°		
Search (m): major/semimajor/minor ("vertical")	20 / 20 / 20		
Inverse distance power	4		
High-grade restrictions (grade in ppm Ag and distance in m)	None		



17.6 Resource

The resource was classified to CIM standards. For consistency and a lack of compelling reasons to do otherwise, the resource classification used the same criteria as the previous estimate, except that MDA considered that some material should be classified as Measured. Because copper adds the greatest value to the deposit, all classification is based on the copper while gold and silver are carried along with the copper. The classification is demonstrated in Table 17.6. While there is gold in the leached zone, all blocks in the leached zone are unclassified for metallurgical reasons and there is no plan to extract gold from the leached zone.

All – Measured

Minimum no. of samples /minimum no. of holes / maximum distance (m) 2 / 1 / 20

Hypogene – Indicated

Minimum no. of samples /minimum no. of holes / maximum distance (m) 2 / 2 / 100

Or

Minimum no. of samples /minimum no. of holes / maximum distance (m) 2 / 1 / 35

Enriched (supergene) and Mixed – Indicated

Minimum no. of samples /minimum no. of holes / maximum distance (m) 2 / 2 / 75

Or

Table 17.6 Criteria for Resource Classification

The inclusion of Measured material in this resource update demonstrates an increased level of confidence, conveyed by the observations that a) the geology is relatively well understood; b) grade continuity is good; c) the deposit is relatively predictable; and d) the sampling is of good quality. On the other hand, the relatively small amount of Measured material (~15% of the total Measured and Indicated) is a consequence of the need to portray some of the risks incorporated in the model, which are the consequence of these facts:

All material not classified above is <u>Inferred</u>

Leached – modeled but unclassified; all Leached material is considered to be waste

- estimation of the volumes of the vertical dikes and breccias is risky, because the majority of the drill holes were vertical;
- the check sampling on gold grades demonstrates only modest reproducibility; and
- there are no down-hole surveys for 50 of the drill holes.

Minimum no. of samples /minimum no. of holes / maximum distance (m)

The resource tabulation is presented in Tables 17.7 to 17.10. Table 17.11 compares the 2004 and 2005 resource estimates. The increase in Indicated tonnes (and the inclusion of Measured tonnes) was a direct result of the 2005 drilling. The decrease in Inferred tonnes (aside from moving into Indicated or Measured) was a direct result of the 2005 drilling better defining the extents of the mineralization, which in the modeling work, stopped the higher grades from extending as far outward on the edges of the model. The overall decrease in higher-grade tonnes is a function of the updated zones and grade shells, the grades reported in the new drilling, the incorporation of dilution factors, and, to a lesser extent, modifications to the estimation procedures. Table 17.12 presents the differences in the estimated resources inside the AMEC-designed pit.

2/1/35



Table 17.7 Mirador Copper, Gold and Silver Resources – Measured

Total Measured

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.30	62,680,000	0.60	831,000,000	200	400,000	1.5	3,080,000
0.35	57,610,000	0.63	795,000,000	200	380,000	1.6	2,930,000
0.40	52,610,000	0.65	753,000,000	210	360,000	1.6	2,770,000
0.45	47,900,000	0.67	709,000,000	220	330,000	1.7	2,590,000
0.50	42,810,000	0.69	656,000,000	220	310,000	1.7	2,370,000
0.55	36,620,000	0.72	584,000,000	230	270,000	1.8	2,090,000
0.60	30,360,000	0.75	505,000,000	240	230,000	1.8	1,790,000
0.65	24,440,000	0.79	424,000,000	240	190,000	1.9	1,480,000
0.70	18,140,000	0.83	330,000,000	250	150,000	1.9	1,130,000
0.75	11,950,000	0.88	231,000,000	260	100,000	2.0	769,000
0.80	7,910,000	0.93	162,000,000	270	68,000	2.1	522,000
0.85	5,090,000	0.99	111,000,000	270	44,000	2.1	340,000
0.90	3,220,000	1.06	75,000,000	290	30,000	2.1	215,000
0.95	2,000,000	1.14	50,000,000	300	20,000	2.0	131,000
1.00	1,470,000	1.21	39,000,000	310	15,000	2.0	97,000

Cutoff in %Cu

Table 17.8 Mirador Copper, Gold and Silver Resources - Indicated

Total Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.30	491,510,000	0.55	5,958,000,000	180	2,810,000	1.4	21,970,000
0.35	441,080,000	0.58	5,596,000,000	180	2,610,000	1.4	20,530,000
0.40	385,060,000	0.60	5,134,000,000	190	2,380,000	1.5	18,760,000
0.45	335,680,000	0.63	4,672,000,000	200	2,150,000	1.6	16,890,000
0.50	283,610,000	0.66	4,126,000,000	210	1,890,000	1.6	14,770,000
0.55	230,250,000	0.69	3,507,000,000	210	1,590,000	1.7	12,400,000
0.60	176,780,000	0.73	2,831,000,000	220	1,260,000	1.7	9,910,000
0.65	129,500,000	0.76	2,181,000,000	230	950,000	1.8	7,560,000
0.70	90,220,000	0.80	1,598,000,000	240	680,000	1.9	5,420,000
0.75	55,700,000	0.85	1,047,000,000	240	435,000	1.9	3,441,000
0.80	33,300,000	0.91	666,000,000	250	270,000	2.0	2,124,000
0.85	18,670,000	0.97	401,000,000	260	157,000	2.0	1,208,000
0.90	10,700,000	1.05	248,000,000	270	92,000	2.1	710,000
0.95	6,650,000	1.13	165,000,000	270	57,000	2.1	452,000
1.00	4,550,000	1.20	120,000,000	270	40,000	2.1	308,000

Cutoff in %Cu



Table 17.9 Mirador Copper, Gold and Silver Resources - Measured and Indicated

Total Measured and Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.30	554,190,000	0.56	6,789,000,000	180	3,210,000	1.4	25,050,000
0.35	498,690,000	0.58	6,391,000,000	190	2,990,000	1.5	23,460,000
0.40	437,670,000	0.61	5,887,000,000	190	2,740,000	1.5	21,530,000
0.45	383,580,000	0.64	5,381,000,000	200	2,480,000	1.6	19,480,000
0.50	326,420,000	0.66	4,782,000,000	210	2,200,000	1.6	17,140,000
0.55	266,870,000	0.70	4,091,000,000	220	1,860,000	1.7	14,490,000
0.60	207,140,000	0.73	3,336,000,000	220	1,490,000	1.8	11,700,000
0.65	153,940,000	0.77	2,605,000,000	230	1,140,000	1.8	9,040,000
0.70	108,360,000	0.81	1,928,000,000	240	830,000	1.9	6,550,000
0.75	67,650,000	0.86	1,278,000,000	250	535,000	1.9	4,210,000
0.80	41,210,000	0.91	828,000,000	260	338,000	2.0	2,646,000
0.85	23,760,000	0.98	512,000,000	260	201,000	2.0	1,548,000
0.90	13,920,000	1.05	323,000,000	270	122,000	2.1	925,000
0.95	8,650,000	1.13	215,000,000	280	77,000	2.1	583,000
1.00	6,020,000	1.20	159,000,000	280	55,000	2.1	405,000

Cutoff in %Cu

Table 17.10 Mirador Copper, Gold and Silver Resources -Inferred

Total Inferred

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.30	417,300,000	0.45	4,124,000,000	150	1,960,000	1.1	15,130,000
0.35	338,390,000	0.48	3,559,000,000	150	1,670,000	1.2	13,220,000
0.40	235,400,000	0.52	2,708,000,000	170	1,250,000	1.3	9,900,000
0.45	175,230,000	0.56	2,147,000,000	180	980,000	1.4	7,820,000
0.50	122,290,000	0.59	1,593,000,000	180	710,000	1.5	5,790,000
0.55	70,270,000	0.64	993,000,000	190	440,000	1.5	3,470,000
0.60	37,890,000	0.71	587,000,000	190	230,000	1.6	1,970,000
0.65	22,020,000	0.76	369,000,000	190	140,000	1.7	1,200,000
0.70	14,710,000	0.81	260,000,000	190	90,000	1.8	824,000
0.75	9,450,000	0.85	177,000,000	200	60,000	1.9	561,000
0.80	5,750,000	0.90	114,000,000	210	39,000	2.0	370,000
0.85	4,020,000	0.93	82,000,000	210	28,000	2.1	266,000
0.90	2,530,000	0.96	54,000,000	210	17,000	2.1	170,000
0.95	1,290,000	1.00	28,000,000	220	9,000	2.2	90,000
1.00	530,000	1.04	12,000,000	220	4,000	2.2	38,000

Cutoff in %Cu

^{*}total Measured plus Indicated were calculated from rounded Measured and rounded Indicated resources and hence some apparent differences are rounding related.



Table 17.11 Comparison of 2005 and 2004 (AMEC) Resource Estimates

AMEC

Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.4 Cutoff	309,700,000	0.66	4,485,589,000	201	2,001,000	NA	NA
0.5 Cutoff	262,200,000	0.69	3,976,393,000	211	1,778,000	NA	NA
0.6 Cutoff	189,100,000	0.74	3,084,654,000	221	1,342,000	NA	NA
0.7 Cutoff	107,600,000	0.81	1,930,789,000	241	832,000	NA	NA

AMEC

Inferred

	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.4 Cutoff	315,100,000	0.56	3,897,292,000	170	1,725,000	NA	NA
0.5 Cutoff	216,500,000	0.62	2,964,790,000	180	1,256,000	NA	NA
0.6 Cutoff	94,200,000	0.71	1,478,052,000	200	606,000	NA	NA
0.7 Cutoff	41,200,000	0.79	721,257,000	230	305,000	NA	NA

Change from AMEC 2004 to MDA 2005

Measured and Indicated

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	41%	-7%	31%	-5%	37%	NA	NA
0.50	24%	-3%	20%	0%	24%	NA	NA
0.60	10%	-1%	8%	0%	11%	NA	NA
0.70	1%	-1%	0%	0%	0%	NA	NA

Change from AMEC 2004 to MDA 2005

Inferred

Cutoff	Tonnes	Cu (%)	lbs Cu	Au (ppb)	oz Au	Ag (ppm)	oz Ag
0.40	-25%	-7%	-31%	0%	-28%	NA	NA
0.50	-44%	-5%	-46%	0%	-43%	NA	NA
0.60	-60%	-1%	-60%	-5%	-62%	NA	NA
0.70	-64%	2%	-64%	-18%	-70%	NA	NA



Table 17.12 Comparison of 2005 and 2004 (AMEC) Resource Estimates – Inside AMEC Pit

	MDA M+I M	odel within	AMEC 200	04 Pit Desig	n	
	Tonnes	Cutoff	Cu grade	Au grade	Cu	Au
Phase	kt	Cu %	Cu %	g/t	kt	ozs (000)
1	39,746	0.44	0.755	0.232	300	296
2	29,547	0.41	0.637	0.199	188	189
3	44,132	0.35	0.603	0.198	266	282
Total	113,425		0.665	0.210	754	767
	MDA Inferred	Model with	nin AMEC 2	2004 Pit Des	ign	
	Tonnes	Cutoff	Cu grade	Au grade	Cu	Au
Phase	kt	Cu %	Cu %	g/t	kt	ozs
1	503	0.44	0.629	0.184	3	3
2	224	0.41	0.626	0.158	1	1
3	1,051	0.35	0.528	0.129	6	4
Total	1,778		0.569	0.148	10	8
Waste (include	s Inferred)					
Phase	kt					
1	35,664					
2	18,277					
3	34,820					
Total	88,761					

	AMEC	Reported	Indicated 7	Tonnes		
	Tonnes	Cutoff		Au grade	Cu	Au
Phase	kt	Cu %	Cu %	g/t	kt	ozs (000)
1	38,294	0.44	0.751	0.241	288	297
2	29,807	0.41	0.635	0.211	189	202
3	42,526	0.35	0.617	0.198	262	271
Total	110,627		0.668	0.216	739	770
	AME	C Reported	I Inferred T	onnes		
	Tonnes	Cutoff	Cu grade	Au grade	Cu	Au
Phase	kt	Cu %	Cu %	g/t	kt	ozs
1	2,407	0.44	0.683	0.228	16	18
2	2,330	0.41	0.533	0.191	12	14
3	5,057	0.35	0.458	0.166	23	27
Total	9,794		0.531	0.187	52	59
Waste (include	s Inferred)					
Phase	kt					
1	35,836					
2	18,022					
3	37,314					
Total	91,172					

It is important to note that:

- The deepest drill holes extend to the ~850 m elevation, and are also mineralized;
- The lowest estimated Indicated material is at ~750 m;
- MDA modeled to 650 m; and
- "Reasonable but optimistic" pit optimization parameters yield a pit that goes to ~750 m on Measured and Indicated material only.

Consequently, MDA has reported resources to the 750 m elevation and no deeper in spite of the indications that the mineralization is open to depth. Pit optimization shells bottom out at 650 m (the bottom of the estimated model) when considering the Inferred material in the pit optimization and using "reasonable but optimistic" pit optimization parameters, 200 m below the deepest drill intercept.



Checks were made on the model in the following manner:

- Cross sections with the zones, drill hole assays and geology, topography, sample coding, and block grades with classification were plotted and reviewed for reasonableness;
- Block model information, such as coding, number of samples, and classification were checked by zone and lithology on a bench-by-bench basis on the computer;
- Quantile-quantile plots of assays, composites, and block model grades were made to evaluate differences in distributions of metals;
- The updated model and estimation parameters were compared to the previous model (Table 8.6) and estimation parameters⁷; and
- Multiple estimation iterations were done comparing the models with and without the 2005 drill holes as well as changing the estimation parameters.

It became evident from comparing the models that several factors impacted the 2005 model relative to the 2004 model. These are described in order of decreasing impact.

- 1. The greatest impact on the changes to estimated resources was caused by more rigid controls on the estimation through the use of better-defined grade and lithologic shells manually modeled rather than indicator modeled.
- 2. The 2005 drill holes, which were located principally along the margins of the deposit, had the effect of limiting the projection of the higher grades and decreasing the mean grade of the resource. The 2005 drilling was the only reason for the large increase in Indicated material. The new drilling and continued efforts by Corriente allow for the inclusion of Measured material in this resource estimate update.
- 3. The incorporation of dilution along the margins of the mineralized material affected the overall grade in a negative way, thereby more closely approaching what will be mined on blocks of 15 m by 15 m.
- 4. The change from ID⁸ to ID⁴ reduced the tonnage of the higher-grade (over ~0.7%Cu) material due to allowing for some grade averaging (smoothing) during estimation.

17.7 Discussion, Qualifications, Risk and Recommendations

The most important observation that can be presented to the reader is the likelihood that geological reality is more complex with respect to breccias and dikes than is portrayed in the resource model. This could have an effect (assuming perfect grade control) of presenting the mill with less tonnes at higher grade during production. Other noteworthy points are presented below.

Vertical dikes and breccias Corriente has begun drilling more angle holes minimizing the risks associated with the vertical drill holes and vertical post- and syn-mineralization dikes and breccias. A certain amount of risk remains in this resource estimate because of the inability to fully assess location, quantity and width of the near vertical dikes and breccias.

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⁷ Note that there is an increase in total tons for all categories at a cutoff of 0.4%Cu of 50 million.



Solids While Corriente made valiant efforts at making solids to define the dikes and breccias, the solids contained numerous variably overlapping volumes of space within their geometries. Because the solids were not modeled so that any given space is only occupied by one solid, a certain number of "workarounds" were necessary in the modeling process. While MDA believes that there are no material errors or biases instilled in this model by modeling on screen and directly via solids, a cross-sectional model taken to plan would have added confidence, precision, and accuracy.

Corriente should take the time to slice the lithology and grade shell solids to section and plan, and edit accordingly to produce non-overlapping interpretations, as well as to refine inaccurate geometries introduced by the solids modeling. If the sections and plans remain relatively simple, then the solids could be reconstructed from the validated and modified level plans.

Sample Grade Reproducibility Rather large discrepancies exist in gold pulp duplicate assays and larger discrepancies exist in the coarse reject duplicate assays. Likely, this reproducibility would be worse at the core sample splitting stage. The information does not imply an inherent bias, as the overall mean gold grade should be correct. MDA suggests that a small program (about fifty samples) of metallic screen assaying be done in order to make a preliminary assessment of the reproducibility of gold grades, optimum sample sizes, and sub-sampling procedures.

Modeling Future modeling should consider using a partial-block model instead of a sub-block model, which would require valid and non-overlapping solids or taking the model to plan levels matching the block height.

Other Metals Additional study is warranted to assess the possibility and magnitude of mobilization and potential enrichment of silver mineralization. While this does not appear to be of great importance, as silver provides relatively small amounts of value in the overall economics of the deposit, it is worthy of a modest study to assess this and determine if modeling should be done differently. Future study and possible estimation should be focused on the modes of occurrence of molybdenum and zinc (and other elements) as providing some potential economic impact, positive (*e.g.*, molybdenum) or negative (*e.g.*, zinc).



18.0 OTHER RELEVANT DATA AND INFORMATION

18.1 Introduction

MDA generated a series of floating cone pit shells from the MDA Measured and Indicated resource described in this report using the AMEC May, 2005 *Mirador Copper Project Feasibility Study* economics and pit slope angles. Two production schedules were generated from the \$1.00 per pound copper price pit shell. The first schedule assumed 25,000 tonnes per day to the mill for the life of the mine and the second schedule started with 25,000 tonnes per day, which was increased to 50,000 tonnes per day in year 6. Corriente personnel then created financial models using these production schedules.

In the AMEC feasibility study the ultimate pit size was limited to a total of 110 million "ore" tonnes, which equates to about a 12-year mine life at 25,000 "ore" tonnes per day. MDA did not restrict the pit size due in part to a change in the maximum pit wall height and therefore the comparable pit shell is significantly larger. Note the use of the term "ore" is taken from the AMEC feasibility report.

18.2 Floating Cone Analyses

MDA used the MineSight® Lerchs-Grossmann "floating cone" algorithm to produce open-pit cone shells using the parameters shown in Table 18.1. All of these physical and economic parameters are the same as the ones in the AMEC feasibility study. Only Measured and Indicated materials were allowed to make positive economic contributions; Inferred material was considered waste. Net block values were calculated for, and coded into each block in the model below topography, with waste blocks receiving negative numbers equivalent to the cost of mining. The same calculations were used to determine the cutoff between mill feed and waste. The resulting cutoff grade for the base case (\$1.00/lb Cu price), assuming only copper revenue, is 0.37% Cu. Because recovered gold contributes value, the actual cutoff is slightly lower depending on the gold grade. Multiple cone runs were made to test for sensitivity to metals prices and the results are summarized in Table 18.2.



Table 18.1 Floating Cone Parameters

Item	Va	lue
Copper Processing		
Mill recovery %		91.4%
Concentrate grade %		30%
Concentrate moisture %		8%
Concentrate losses %		0.25%
Concentrate transport \$/WMT	\$	81.62
Concentrate transport \$/DMT	\$	88.72
Smelting \$/DMT	\$	75.00
Smelter recovery %		96.5%
Refining \$/lb	\$	0.08
Gold Processing		
Mill recovery %		47%
Smelter payable %		95%
Refining \$/oz	\$	6.00
Process cost with G&A \$/DMT	\$	3.90
Mining \$/DMT	\$	0.89
Copper price \$/lb	\$0.6	5-\$1.50
Gold price \$/oz		\$400
Overall pit slope angles		35°-42°
DMT = Dry Metric Tonne		
WMT = Wet Metric Tonne		

Table 18.2 Floating Cone Results

Cu price	Tonnes > cu	t (Measured	d & Indicate	d only)	Waste tns	Total tns	
\$/lb	x1000	Cu %	Au g/t	Ag g/t	x1000	x1000	strip ratio
\$0.65	5,178	1.12	0.249	1.89	11,149	16,327	2.15
\$0.70	13,070	0.93	0.258	1.81	16,673	29,743	1.28
\$0.75	39,203	0.81	0.242	1.89	41,073	80,276	1.05
\$0.80	77,386	0.74	0.228	1.85	77,662	155,048	1.00
\$0.85	156,852	0.69	0.217	1.74	204,306	361,158	1.30
\$0.90	242,767	0.66	0.207	1.67	336,497	579,264	1.39
\$0.95	291,052	0.64	0.201	1.62	394,849	685,901	1.36
\$1.00	346,995	0.62	0.196	1.57	491,393	838,388	1.42
\$1.05	388,341	0.60	0.192	1.52	556,834	945,175	1.43
\$1.10	416,382	0.59	0.188	1.49	587,276	1,003,658	1.41
\$1.15	440,912	0.58	0.185	1.47	612,894	1,053,806	1.39
\$1.20	464,423	0.57	0.183	1.44	647,144	1,111,567	1.39
\$1.25	487,622	0.56	0.180	1.42	681,837	1,169,459	1.40
\$1.30	503,816	0.55	0.178	1.41	698,646	1,202,462	1.39
\$1.35	520,022	0.54	0.176	1.39	710,333	1,230,355	1.37
\$1.40	534,064	0.54	0.174	1.38	738,935	1,272,999	1.38
\$1.45	544,040	0.53	0.173	1.37	755,431	1,299,471	1.39
\$1.50	551,465	0.53	0.172	1.36	763,612	1,315,077	1.38



Slope angles varied by sector as follows (from AMEC feasibility).

For feasibility purposes, the following inter-ramp slopes are recommended by zone (where 0° due North, 90° due East):

Zone I (330° to 60°)	35°
Zone II (60° to 150°)	42°
Zone III (150° to 180°)	40°
Zone IV (180° to 270°)	38°
Zone V (270° to 330°)	40°

The slopes suggested above are preliminary estimates only and may be modified with additional geotechnical drilling, during subsequent design work and trial excavations during the early stages of mining.

Work done by Piteau Associates, a geotechnical consulting firm based in Vancouver B.C., after the AMEC feasibility was completed, indicated that the overall pit depth restriction of 500m can be eliminated if 30m wide catch benches are placed in the slope every 200m of elevation. Specifically, Zones III and IV would have slopes higher than 500m and would require the extra catch benches. The overall slope angles updated by Piteau are slightly steeper than the AMEC angles but the AMEC angles were used in the floating cones to be consistent with the AMEC work. Piteau is in the process of finalizing their work and refinements to the slope angles and design criteria are possible.

18.3 Production Schedules

MDA divided the ultimate pit shell into four phases in order to approximate the phases of a designed pit. The floating cone shell at a copper price of \$0.72 per pound, containing 43 million total tonnes, was used as a starter pit. Subsequent phase shells were at least 100 m from the previous shell to allow enough potential mining width. Phase 2 contains 112 million tonnes, phase 3 contains 206 million tonnes and phase 4 contains 477 million tonnes. Two production schedules were created; the first at 25,000 tonnes per day (tpd) mill feed and the second starting at 25,000 mill tonnes per day increasing to 50,000 tonnes per day in year 6. The schedules are shown in Table 18.3 and Table 18.4.

Table 18.3 25,000 Tonnes per Day Production Schedule

Period (year)	-1	1	2	3	4	5	6	7	8	9	10	11	12	
Mill kt	0	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	
Cu grade %	0.000	0.852	0.765	0.729	0.633	0.599	0.606	0.582	0.560	0.597	0.615	0.612	0.637	
Au grade g/t	0.176	0.219	0.240	0.252	0.230	0.221	0.180	0.187	0.203	0.226	0.228	0.193	0.207	
Ag grade g/t	1.52	1.88	1.63	1.68	2.09	1.93	1.87	1.75	1.40	1.48	1.55	1.49	1.61	
Waste kt	5,000	11,341	6,189	15,811	18,250	18,935	9,125	10,912	11,552	9,125	10,577	5,418	42,007	
Period (year)	13	14	15	16	17	18	19	20	21	22	23	24	25	
Mill kt	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	
Cu grade %	0.680	0.677	0.619	0.598	0.589	0.596	0.617	0.645	0.628	0.500	0.501	0.548	0.562	
Au grade g/t	0.213	0.213	0.182	0.166	0.173	0.191	0.197	0.193	0.181	0.176	0.190	0.204	0.206	
Ag grade g/t	1.62	1.85	1.61	1.70	1.87	1.74	1.46	1.59	1.51	1.13	1.16	1.25	1.21	
Waste kt	13,036	10,356	10,869	15,330	9,125	9,125	9,125	9,125	37,680	45,884	21,036	18,122	15,841	
Period (year)	26	27	28	29	30	31	32	33	34	35	36	37	38	39
Mill kt	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	9,125	218
Cu grade %	0.583	0.594	0.599	0.606	0.615	0.631	0.622	0.613	0.627	0.621	0.621	0.599	0.579	0.581
Au grade g/t	0.202	0.195	0.187	0.178	0.174	0.181	0.184	0.186	0.193	0.199	0.195	0.164	0.126	0.117
Ag grade g/t	1.26	1.37	1.54	1.60	1.68	1.64	1.58	1.68	1.58	1.47	1.46	1.38	1.24	1.13
Waste kt	13,998	14,456	12,640	9,088	7,663	6,489	5,488	4,966	4,036	3,235	2,648	2,704	5,032	82



Table 18.4 50,000 Tonnes per Day Production Schedule

Period (year)	-1	1	2	3	4	5	6	7	8	9	10	
Mill kt	0	9,125	9,125	9,125	9,125	9,125	18,250	18,250	18,250	18,250	18,250	
Cu grade %	0.000	0.852	0.765	0.729	0.633	0.599	0.594	0.578	0.624	0.676	0.621	
Au grade g/t	0.176	0.219	0.240	0.252	0.230	0.221	0.184	0.212	0.203	0.218	0.200	
Ag grade g/t	1.521	1.881	1.630	1.676	2.093	1.929	1.807	1.436	1.550	1.715	1.604	
Waste kt	5,000	11,341	6,189	15,811	18,250	18,935	20,037	19,919	4,755	40,159	21,225	
Period (year)	11	12	13	14	15	16	17	18	19	20	21	22
Mill kt	18,250	18,250	18,250	18,250	18,250	18,250	18,250	18,250	18,250	18,250	18,250	9,343
Cu grade %	0.594	0.608	0.635	0.500	0.555	0.589	0.603	0.623	0.617	0.624	0.610	0.579
Au grade g/t	0.170	0.194	0.187	0.183	0.205	0.198	0.183	0.178	0.185	0.196	0.179	0.126
Ag grade g/t	1.784	1.601	1.551	1.145	1.231	1.318	1.566	1.661	1.633	1.526	1.417	1.236
Waste kt	40,250	55,021	55,021	33,021	33,963	28,454	21,728	14,153	10,453	7,271	5,356	5,109

18.4 Economic Model

Corriente developed an economic model from the AMEC economic model used in their feasibility study. While MDA did not take part in creating the model MDA did review the model and input values. The calculations were consistent between the Corriente model and the AMEC feasibility model and the input costs were the same with the exception of metals prices and capital costs. The most significant differences were the production schedules; Corriente used the schedules in Table 18.3 and Table 18.4 which have longer mine lives than the feasibility schedule. The inputs are summarized in Table 18.5 and results are shown in Table 18.6 and Table 18.7.



Table 18.5 Economic Model Inputs

Base Case	Со	rriente		AMEC
Item	\	/alue	,	Value
Cu price US\$/lb	\$	1.10	\$	1.00
Au price US\$/oz	\$	425	\$	400
Ag price US\$/oz	\$	6.50	\$	6.50
Cu mill recov		91%		91%
Au mill recov		47%		47%
Processing cost US\$/t (LOM)	\$	2.96	\$	2.87
G&A cost US\$/t (LOM)	\$	0.64	\$	0.64
Mining cost US\$/t (LOM)	\$	1.14	\$	1.14
Concentrate Grade		29.9%		29.8%
Moisture		8.0%		8.0%
Land Conc freight (US\$/wmt)		\$35.82		\$35.82
Port Charges (US\$/wmt)		\$2.00		\$1.70
Ocean freight (US\$/wmt)		\$42		\$42
Total freight charges (US\$/wmt)		\$80		\$79.52
Con Treatment Charge US\$/dmt		\$75		\$75
Cu refining Charge US\$/pay lb		\$0.075		\$0.075
Cu pay factor		96.5%		96.5%
Cu Unit Deduction		1.0%		1.0%
Au pay factor		95.0%		95.0%
Au unit deduction		0.0		0.0
Au Refining Charge US\$/troy oz		\$6.00		\$6.00
Ag pay factor		90.0%		90.0%
Ag unit deduction		0.0		0.0
Ag Refining Charge US\$/troy oz		\$0.40		\$0.40
Concentrate Losses		0.25%		0.25%

Table 18.6 Economic Model Results, 25,000 tpd Case (8% discount rate)

			` `
Cι	ı Price	Pre-tax	Pre-tax NPV
U	S\$/lb	IRR %	US\$ millions
\$	1.00	15.8%	111
\$	1.10	22.6%	224
\$	1.20	28.8%	337
\$	1.45	43.1%	620

Cι	ı Price		Cash Flow (US\$ 000's)					
U	S\$/lb	Year 1	Year 2	Year 3	Year 4	Total		
\$	1.00	44,598	55,733	42,819	29,079	172,229		
\$	1.10	56,947	69,326	55,634	40,937	222,844		
\$	1.45	100,171	116,899	100,486	80,009	397,565		
\$	1.75	137,220	157,677	138,931	113,961	547,789		



Table 18.7 Economic Model Results, 50,000 tpd Case (8% discount rate)

Cu Price		Pre-tax	Pre-tax NPV
U	S\$/lb	IRR %	US \$ millions
\$	1.10	24.0%	349

Based on a study by Merit Consultants International Inc., which is part of the AMEC feasibility study, Corriente estimated initial capital to be US\$195 million for the 25,000 tpd scenario and US\$295 million for the 50,000 tpd scenario. The 50,000 tpd case sees a doubling of plant production capacity in year 5 at an additional capital cost of US\$100 million, incurred in year 5. Table 18.8 is a summary of initial capital for the 25,000 tpd case (the 50,000 tpd case is the same except for the additional US\$100 million capital spent in year 5).

Table 18.8 25,000 tpd Case Initial Capital

Area	Cost (US\$ x1000)
Direct Costs	
Mine	\$11,108
Process Plant	\$87,922
Utilities	\$6,920
Site Preparation and Roads	\$13,561
Tailings	\$8,474
Ancillary Facilities	\$3,847
Total Direct Costs	\$131,832
Indirect Costs	
Project Indirects	\$39,362
Owner Indirects (includes BHP royalty buyout)	\$6,376
Total Indirect Costs	\$45,738
Subtotal	\$177,570
Contingency	\$17,735
Total Project	\$195,305



19.0 REQUIREMENTS FOR TECHNICAL REPORTS ON PRODUCTION AND DEVELOPMENT PROPERTIES

AMEC Americas Ltd completed a feasibility study on the Mirador property titled "Mirador Copper Project Feasibilty Study Report" in May 2005. Corriente filed that study on the SEDAR website on May 13, 2005, and the study is available on the Corriente website, http://www.corriente.com. MDA reviewed sections of the feasibility relating to mining and mining-related economics and believes the information provided to be reasonable and generally current. The work described in Section 18 of this report was based on information from this AMEC feasibility study.

Excerpts from the feasibility are provided below. Note that the terms "ore", "orebody" and "ore body" used by AMEC in the following are not 43-101 compliant terms in that no reserve has been stated for this deposit.

The feasibility study is based on conventional open pit mining of the porphyry copper deposit. The deposit is covered by an average 22 m depth of overburden and a leached cap, a portion of which must be pre-stripped to access the orebody. The sulphide ore body is relatively homogenous, consisting dominantly of primary copper sulphides and is open at depth. Secondary enrichment is thinly developed in places over the primary sulphide mineralization. Overall, the metallurgy is regarded as relatively simple.

The mine plan is based on a contract mining company providing ore to a conventional copper concentrator to support an average milling rate of 25,000 t/d (9.125 Mt/a). All facilities are designed for this throughput and operate on a continuous basis, 24 h/d, 365 d/a.

Run-of-mine ore will be crushed in a gyratory crusher. The mill flow sheet selected for Mirador will be a conventional copper-gold porphyry flowsheet, with relatively coarse primary semi-autogenous and ball mill grinding to about 150 µm followed by copper rougher flotation, concentrate regrind to 30 µm, and cleaner flotation and dewatering. Concentrates produced are predicted to average 29.8% copper at a recovery of 91%. Gold recovery is expected to average 47%. A laboratory analysis of concentrates indicated that no significant deleterious penalty element impurities are present. The concentrate will be trucked via the existing road network in the area to a port facility in Machala for shipment to smelters. Tailings from the process will be impounded in a zero discharge tailings pond; water will be reclaimed from the tailings pond and reused in the process.

The major infrastructure required to develop the property includes road access upgrades, a runof-river hydroelectric scheme, and power line. The hydroelectric development is not part of the scope of this study and the supply of power will be through an independent build-own-operate arrangement. A 2.7 km access road is needed to connect the plant and administration areas to the existing highway that passes by the property. Access between the plant area and the mine will be via upgraded existing roads including a new 5 km section to the pit area. A 10 km overland conveyor will connect the process plant and the crusher. In addition, a 100 km power line will have to be constructed, as part of the Sabanilla Hydroelectric Project, to connect the site to the hydroelectric power station and the existing power grid. The power demand of the



project is about 28.3 MW. Seasonal variations in the output of the hydroelectric scheme result in an average output of about 23.5 MW and, on average, 4.8 MW of supplementary power will be imported from the existing power grid. [Note the update to the power situation described in Section 5.4.]

Merit Consultants International Inc. (Merit) estimated the capital cost to build the facilities as described in this report to be US\$202 million. Mining costs were based on contract mining budget quotations. Process operating costs and G&A costs were estimated by AMEC with input from Corriente.

Mining at Mirador will be by conventional open pit truck and shovel methods. Budget pricing was obtained for contract mining. The mining fleet is estimated to consist of two 19.9 m3 frontend loaders and eight 140 t trucks. Support equipment will include bulldozers, graders, and excavators to maintain the surfaces of the roads, dumps and operating benches and the water collection system at the pit rim and in-pit.

The parameters used in the detailed pit design, including the geotechnical data described above, are as follows:

•	bench h	height, single benching	12 m
•	berm w	ridth	8 m
•	haul ro	ads and pit ramps	
	-	total width allowance	22 m
	-	running surface	18 m
	-	berms and ditches	4 m
	-	berm access from ramp	bottom only
	_	maximum grade	10%

The current power situation is described in Section 5.4.



20.0 CONCLUSIONS

The last NI 43-101 compliant Technical Report for the Mirador project was filed by AMEC in October 2004. Since that time, Corriente Resources Inc. has advanced the Mirador Project principally with additional drilling but also with additional economic and engineering studies. A number of important studies and work programs have been completed, notably the following:

- A Feasibility Study Report, completed in May 2005 (AMEC Americas Limited));
- A 52-hole, 11,935-m core-drilling program;
- An updated copper, gold, and silver resource estimate and pit optimizations completed in December 2005 (MDA); and
- An Environmental Impact Assessment (EIA) Report with supporting documentation, filed in December 2005.

The May 2005 Feasibility Study Report does not include or address the results of subsequent work programs such as the 2005 drilling program at Mirador, or the results of studies such as the updated copper, gold, and silver resource estimates and pit optimizations completed in December 2005 by MDA. The present Technical Report provides a summary of all work conducted since the inception of the Mirador Project, and an update and review of the Mirador Project activities that took place subsequent to the completion of the Feasibility Study Report.

MDA has reviewed the methodology and results of the 2005 Mirador drilling program. This program included drill holes M91 through M141. The updated drill hole assay database contains 3,592 new assayed drill intervals from these holes. For the 2005 drilling program, Corriente generally followed the quality assurance/quality control (QA/QC) guidelines recommended by AMEC Americas Ltd (AMEC 2004). MDA has reviewed the results of the 2005 Corriente QA/QC program but did not take independent samples from the 2005 drill holes. MDA did take check samples from drilling conducted prior to 2005. The discussion in the following section relates to the 2005 program only.

The sample preparation procedures are appropriate and well done, and the assays and analyses are of good quality. Based on the results of the assays and analyses of standard samples inserted into the sample stream, there does not appear to be any significant bias in the assay or analytical data. The results from the inserted blank samples indicate that the sample preparation procedures are conducted with appropriate care. Copper analyses of pulp duplicates reproduce well, while gold fire assays of pulp duplicates show modest variability. Although MDA and Sivertz do not believe that the modest variability in the reproducibility of gold assays has instilled any material bias or skewed the results, it is suggested that this phenomenon be investigated with a set of metallic screen samples. MDA and Sivertz also recommend that a small percentage of samples be sent "blind" to a second umpire laboratory, as an additional check on the primary laboratory.

MDA completed a resource update for the Mirador Project based on the 52 additional drill holes. MDA relied upon the results of previous work, and used procedures similar to those used by AMEC in the



preparation of the 2004 mineral resource estimate (AMEC 2004). MDA reported Measured and Indicated resources of 437,670,000 tonnes grading 0.61% Cu, 190 ppb gold, and 1.5 ppm silver at a 0.40% Cu cutoff grade. Inferred resources, also at a 0.40% Cu cutoff, were reported to be 235,400,000 tonnes grading 0.52% Cu, 170 ppb gold, and 1.3 ppm silver. The MDA estimate places more material in the Measured and Indicated resource category than was reported by AMEC in 2004, at a slightly lower grade. These changes are the direct result of the addition of new data from the 2005 infill drilling program.



21.0 RECOMMENDATIONS

MDA and Sivertz believe that Mirador is a property of merit. For Mirador specifically, it is recommended that certain work on the resource be completed:

- Make paper cross sectional interpretations through the Mirador deposit that describe and define the rock types, material types, alteration zones, and structure;
- Continue work on the solids using the previously mentioned geologic sections to guide the definition of the rock and material types, and modify the model through various iterations of slicing and reinterpretation;
- With the new material type and rock type models completed, estimate resources using a partial-block model to replace the sub-block model; and
- Estimate zinc grades.

Estimated costs for the previously described resource modeling work would be approximately \$100,000.

In addition, engineering, cost estimation, and environmental/social baseline work should be continued, in order to update the Feasibility Study completed by AMEC Americas Limited. This should involve:

- A review of the proposals received for mine engineering, procurement and construction.
- Studies to determine the optimum production capacity for the Mirador Project, balancing constraints such as availability of electrical power and other logistical realities against maximum achievable mining and milling rates.
- Preparation of an overall mine plan to accommodate expansion to a range of milling capacities from 25,000 tpd to 50,000 tpd.
- Preparation and review of capital expenditure and operating costs for the optimum mine expansion plan.
- Completion of the ongoing slope stability work.
- Additional metallurgical test work to verify that there are not changes to metallurgical characteristics at depth.
- Identification of any potential issues relating to large waste dumps and tailings facilities.

Estimated costs for the previously described engineering work would be approximately \$150,000.

It is further recommended that the Mirador Norte copper deposit should be evaluated from a resource standpoint, using similar procedures to those described above and in other sections of this report. Continued permitting, environmental baseline studies, planning, and pre-production work are all justified.



22.0 REFERENCES

- AMEC Americas Limited, 2005: Mirador Copper Project Feasibility Study Report. May 2005.
- Corriente Resources Inc, 2005: Environmental Impact Assessment for Mirador Project Submitted to Ecuador Government. News Release dated December 20, 2005.
- Corriente Resources Inc, 2005: Mirador Mine Life Extended to 38 Years with New Optimization Results for Starter Copper Project. News Release dated November 17 2005.
- Corriente Resources Inc, 2005: Optimization Drilling Completed at Mirador Project. News Release dated August 8, 2005
- Corriente Resources Inc, 2005: High Grade Copper Intersected at Mirador Project. News Release dated July 6, 2005.
- Corriente Resources Inc, 2005: Optimization Well Underway at Mirador Project, Ecuador. News Release dated May 19, 2005.
- Corriente Resources Inc, 2005: Positive Feasibility Study Completed on Mirador Copper-Gold Starter Project, Southeast Ecuador. News Release dated April 14, 2005.
- Dawson, J.M., and Makepeace, D.K, 2003: Mirador Project, Corriente Copper Belt, Southeast Ecuador. Order-of-Magnitude Study, Part 1, Technical Report. February 2003.
- Lomas, S., 2004: Technical Report, Mirador Project. Morona Santiago Province, Ecuador. AMEC Americas Limited Technical Report prepared for Corriente Resources Inc, October 22 2004.
- Makepeace, D.K, 2001: Corriente Copper Belt Project, Southeast Ecuador, Order-of-Magnitude Study (Preliminary Assessment Technical Report), June 22, 2001.
- Makepeace, D.K, 2002: Mirador Project, Corriente Copper Belt, Southeast Ecuador. Preliminary Assessment Technical Report, September 3, 2002.
- Mineral Development Associates, 2005: Update on Copper, Gold and Silver Resources and Pit Optimizations, Mirador Project, Ecuador. December 6, 2005.
- P&T Asesores Legales, Abogados 2005: Letter Regarding Certain Corporate Matters and the Status of Title to the Mining Concessions in Ecuador. Prepared for Corriente Resources Inc, December 29 2005.

www.aurelian.ca: January 16 2006.



23.0 CERTIFICATE OF QUALIFIED PERSON

- I, Steven Ristorcelli, P. Geo., do hereby certify that:
 - I am currently employed as Principal Geologist by:
 Mine Development Associates, Inc.
 210 South Rock Blvd.
 Reno, Nevada 89502.
 - 2. I graduated with a Bachelor of Science degree in Geology from Colorado State University in 1977 and a Master of Science degree in Geology from the University of New Mexico in 1980.
 - 3. I am a Professional Geologist in the states of California (#3964) and Wyoming (#153) and a Certified Professional Geologist (#10257) with the American Institute of Professional Geologists, and a member of the Geological Society of Nevada, Society for Mining, Metallurgy, and Exploration, Inc., and Prospectors and Developers Association of Canada.
 - 4. I have worked as a geologist for a total of 28 years since my graduation from undergraduate university. Relevant experience includes resource estimation and ancillary work on multitudes of deposits including porphyry copper, molybdenum and gold deposits.
 - 5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
 - 6. I am responsible for or was involved with the preparation of this technical report titled "Technical Report Update on the Copper, Gold, and Silver Resources and Pit Optimizations, Mirador Project, Ecuador" for Corriente Resources Inc. dated May 18, 2006. I visited the project during the period January 4 to January 7, 2005.
 - 7. I have had no prior involvement with the property or project.
 - 8. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
 - 9. I am independent of the issuer applying all of the tests in section 1.4 of National Instrument 43-101.
 - 10. I have read National Instrument 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.



11. I consent to the filing of the Technical Report with any securities regulatory authority, stock exchange and other regulatory authority and any publication by them, including electronic publication of the Technical Report in the public company files on their websites accessible by the public.

Dated this 18th day of May, 2006.

"Steven Ristorcelli"

Signature of Qualified Person

Steven Ristorcelli
Print Name of Qual

Print Name of Qualified Person



- I, George Sivertz, residing at 11708-246th Street, Maple Ridge, BC, V4R 1K8, do hereby certify that:
 - 1. I am currently employed as Senior Geologist by:

OreQuest Consultants Ltd. #306 – 595 Howe Street Vancouver BC, Canada V6C 2T5

- 2. I hold a B.Sc. (Honours) degree in Geological Science granted by the University of British Columbia in 1976.
- 3. I have been a registered member in good standing of the Association of Professional Engineers and Geoscientists of British Columbia since 1992.
- 4. I am a professional geologist and have practiced my profession on a full time basis in Canada, the USA, Mexico, Cuba, Peru, and elsewhere in Europe, Asia, and South America since 1978.
- 5. I have read NI 43-101 and NI 43-101F1 and certify that by reasons of my academic qualifications, affiliation with a professional association, and relevant work experience, I am a "Qualified Person" for the purposes of NI 43-101. This report has been prepared in compliance with NI 43-101.
- 6. I am responsible for or was involved with the preparation of Sections 4.0 to 13.0, inclusive, of this technical report titled "Technical Report Update on the Copper, Gold, and Silver Resources and Pit Optimizations, Mirador Project, Ecuador" for Corriente Resources Inc. May 18th, 2006. I have not visited the Mirador property.
- 7. I am independent of Corriente Resources Inc. and its subsidiary companies. I hold no interests, direct or indirect, in the properties or securities of Corriente Resources Inc. or any of its subsidiary companies, nor do I intend or expect to receive any. I am independent of the issuer applying all of the tests in section 1.4 of National Instrument 43-101.
- 8. I am not aware of any material fact or material change with respect to the subject matter herein, which if omitted could render this report misleading.
- 9. I consent to the filing of the Technical Report with any securities regulatory authority, stock exchange and other regulatory authority and any publication by them, including electronic publication of the Technical Report in the public company files in websites accessible by the public.

Dated this 18 th day of May, 2006.	
"George Sivertz" Signature of Qualified Person	
Signature of Quairied Ferson	
George Sivertz	
Print Name of Qualified Person	



- I, Scott Hardy, P. Eng., do hereby certify that:
 - 1. I am currently employed as Senior Engineer by:

Mine Development Associates, Inc. 210 South Rock Blvd. Reno. Nevada 89502.

- 2. I graduated with a Bachelor of Science degree in General Engineering from Oregon State University in 1978 and Bachelor of Science degree in Geology from the University of Wyoming in 1984.
- 3. I am a Registered Professional Engineer in the state of Nevada (#11891) and a member of the Society for Mining, Metallurgy, and Exploration, Inc.
- 4. I have worked as an engineer for a total of 19 years since my graduation from undergraduate university.
- 5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
- 6. I am responsible for or was involved with the preparation of this technical report titled "Technical Report Update on the Copper, Gold, and Silver Resources and Pit Optimizations, Mirador Project, Ecuador" for Corriente Resources Inc. dated May 18, 2006. I have not visited the Mirador property.
- 7. I have had no prior involvement with the property or project.
- 8. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
- 9. I am independent of the issuer applying all of the tests in section 1.4 of National Instrument 43-101.
- 10. I have read National Instrument 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.



11. I consent to the filing of the Technical Report with any securities regulatory authority, stock exchange and other regulatory authority and any publication by them, including electronic publication of the Technical Report in the public company files on their websites accessible by the public.

Dated this 18 th day of May, 2006.	
"Scott Hardy"	
Signature of Qualified Person	
Scott Hardy	
Print Name of Qualified Person	

CERTIFICATE OF QUALIFIED PERSON

I, John R. Hoffert, P.Eng., do hereby certify that:

1. I am currently an independent Metallurgical Engineer, president and owner of:

Hoffert Processing Solutions Inc.

93 Fairview Drive Williams Lake, B.C., Canada V2G 4K9

- 2. I graduated from the University of British Columbia in 1984 with a Bachelor of Applied Science degree in Mining and Mineral Processing and also hold a Diploma of Technology in Extractive Metallurgy from the British Columbia Institute of Technology obtained in 1975.
- 3. I am a registered Professional Engineer in the province of British Columbia, Canada (#16726) and a long time member of the Canadian Institute of Mining and Metallurgy
- 4. I have worked as a metallurgical engineer for a total of 22 years since my graduation from university and have served in various roles in the mining industry for 31 years.
- 5. I have read the definition of "Qualified Person" set out in National Instrument 43-101 ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for the purposes of NI 43-101.
- 6. I am responsible for or was involved with the preparation of Section 16 of this technical report titled "Technical Report Update on the Copper, Gold, and Silver Resources and Pit Optimizations, Mirador Project, Ecuador" for Corriente Resources Inc. May 18th, 2006.
- 7. I have read the technical feasibility study for the Mirador Copper Project Feasibility Study Report, dated May 2005 and I am familiar with the metallurgical statements made in the report. I visited the project site on May 1, 2 and 3, 2006 and have personally examined the drill core and found the volume and length of the drill core, the copper mineral characterization and apparent fracture hardness in the drill core to be consistent with the conclusions drawn from the test work in the metallurgical study.
- 8. I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission of which to disclose would make the Technical Report misleading.
- 9. I am independent of the issuer applying all of the tests in section 1.4 of National Instrument 43-101.

- 10. I have read National Instrument 43-101 and Form 43-101F1, and this Technical Report has been prepared in compliance with that instrument and form.
- 11. I consent to the filing of the Technical Report with any securities regulatory authority, stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public, of the Technical Report.

Dated this 18th day of May, 2006.

Signature of Qualified Person

John R. Hoffert, P.Eng.

Print Name of Qualified Person

Appendix A

Land Tenure Report by P&T Asesores Legales, Abogados including Map and Tables

P&T ASESORES LEGALES

ABOGADOS

Quito, December 29, 2005

Corriente Resources Inc.
Desjardins Securities Inc.
Canaccord Capital Corporation
CIBC World Markets Inc.
Sprott Securities Inc.
Wellington West Capital Markets Inc.
Lang Michener LLP
Bull, Housser & Tupper LLP

Dear sirs, MINERA CURIGEM S.A.

You have asked us to provide you with our opinion regarding certain corporate matters and the status of title to the mining concessions in Ecuador listed in Annex A. In order to provide the requested opinions, we have reviewed the corporate records of MINERA CURIGEM S.A and such other documents and considered such matters of law as we have considered necessary.

Based on our review, we are of the opinion that:

- MINERA CURIGEM S.A. (Hereinafter referred to as "MCSA") has been duly incorporated for an unlimited duration and is validly existing and in good standing under the laws of Ecuador.
- MCSA has the corporate power and capacity to own, lease and operate its properties and assets and conduct its business as currently carried on.
- The authorized capital of MCSA consists of USD\$ 10.000 and the issued capital of MCSA consists of USD\$ 5.000.
- Corriente Resources Inc., a British Columbia company, is the registered holder of all of the shares in the capital of MCSA
- Based entirely on the search at the following public entities of the Republic of Ecuador. Court Registry, Mercantile Registry; Companies Superintendence; and the Social Books of MINERA CURIGEM S.A. maintained by Ramiro Campos, there are no actions, suits or proceedings pending against or affecting MCSA in Ecuador as at the close of business on December 22, 2005.
- 6. Based on a review of the Mining Title for each mining concession issued by the National Mining Office, which is a department of the Ministry of Energy and Mines in charge of managing the processes of issuance, conservation and extinction of mining rights in accordance with the current mining laws and regulations of Ecuador (the "Mining Law"), each of the properties, as illustrated in the attached map, Annex B (the "Properties"), is duly registered in the name of MCSA.



P&T ASESORES LEGALES

ABOGADOS

- 7. In regards to the status of Title of the mining concessions, each of the Properties is in good standing until the date of expiration of registration listed opposite its name in the attached Annex A. Please note, however, that the term of some of the mining concessions have been suspended by the mining authorities at the owner's request, as listed therein, since physical access to the areas is not possible due to force majeure causes. The suspended status can be removed by the owner at any time and does not affect its title to the mining concessions or mean that they are not in good standing.
- 8. Owners of mining concessions must pay in advance for each mining hectare an annual conservation patent fee for each calendar year, which fee is payable during the month of March. Upon payment of the required annual fee by the renewal date for that concession set forth in Annex A, the registration of each of the Properties will be renewed for another one-year term in the name of its present holder.

Other than the expiration of the term of the concession registered against the title as described in this paragraph 8, lack of such payment is, according to the Mining Law, the only means by which a concession holder may lose its registration to a property. This letter makes no assessment or contains any opinion regarding issues related to the operation of the concessions. All matters related to the operation of the concessions, such as environmental issues, community relations, filing of environmental and other required reports, completion of environmental plans, among others, have been managed through ECUACORRIENTE S.A. and therefore we cannot give an opinion in such regard.

 According to the Mining Law, concessions registered against title to mining properties have a term of 30 years which can be automatically renewed for further successive 30-year periods, provided that before expiration a written notice of renewal is given by the concession holder.

Please don't hesitate to contact me if you have any additional inquiries.

Sincerely yours,

Dr. Juan Xayier Trejo LAWYER AT LAW

P&T ASESORES LEGALES ABOGADOS

Quito, December 29, 2005

Corriente Resources Inc.
Desjardins Securities Inc.
Canaccord Capital Corporation
CIBC World Markets Inc.
Sprott Securities Inc.
Wellington West Capital Markets Inc.
Lang Michener LLP
Bull, Housser & Tupper LLP

Dear sirs, ECUACORRIENTE S.A.

You have asked us to provide you with our opinion regarding certain corporate matters and the status of title to the mining concessions in Ecuador listed in Annex A. In order to provide the requested opinions, we have reviewed the corporate records of **ECUACORRIENTE S.A** and such other documents and considered such matters of law as we have considered necessary.

Based on our review, we are of the opinion that:

- ECUACORRIENTE S.A. (hereinafter referred to as "ESA") has been duly incorporated for an unlimited duration and is validly existing and in good standing under the laws of Ecuador.
- ESA has the corporate power and capacity to own, lease and operate its properties and assets and conduct its business as currently carried on.
- The authorized capital of ESA consists of USD\$ 5.000 and the issued capital of ESA consists of USD\$ 2.000.
- Corriente Resources Inc., a Caymans Islands company, is the registered holder of all of the shares in the capital of ESA.
- Based entirely on the search at the following public entities of the Republic of Ecuador: Court Registry, Mercantile Registry; Companies Superintendence; and the Social Books of ECUACORRIENTE S.A. maintained by Ramiro Campos, there are no actions, suits or proceedings pending against or affecting ESA in Ecuador as at the close of business on December 22, 2005.
- 6. Based on a review of the Mining Title for each mining concession issued by the National Mining Office, which is a department of the Ministry of Energy and Mines in charge of managing the processes of issuance, conservation and extinction of mining rights in accordance with the current mining laws and regulations of Ecuador (the "Mining Law"), each of the properties, as illustrated in the attached map, Annex B (the "Properties"), is duly registered in the name of ESA.



P&T ASESORES LEGALES

ABOGADOS

- In regards to the status of Title of the mining concessions, each of the Properties is in good standing until the date of expiration of registration listed opposite its name in the attached Annex A.
- 8. Owners of mining concessions must pay in advance for each mining hectare an annual conservation patent fee for each calendar year, which fee is payable during the month of March. Upon payment of the required annual fee by the renewal date for that concession set forth in Annex A, the registration of each of the Properties will be renewed for another one-year term in the name of its present holder.

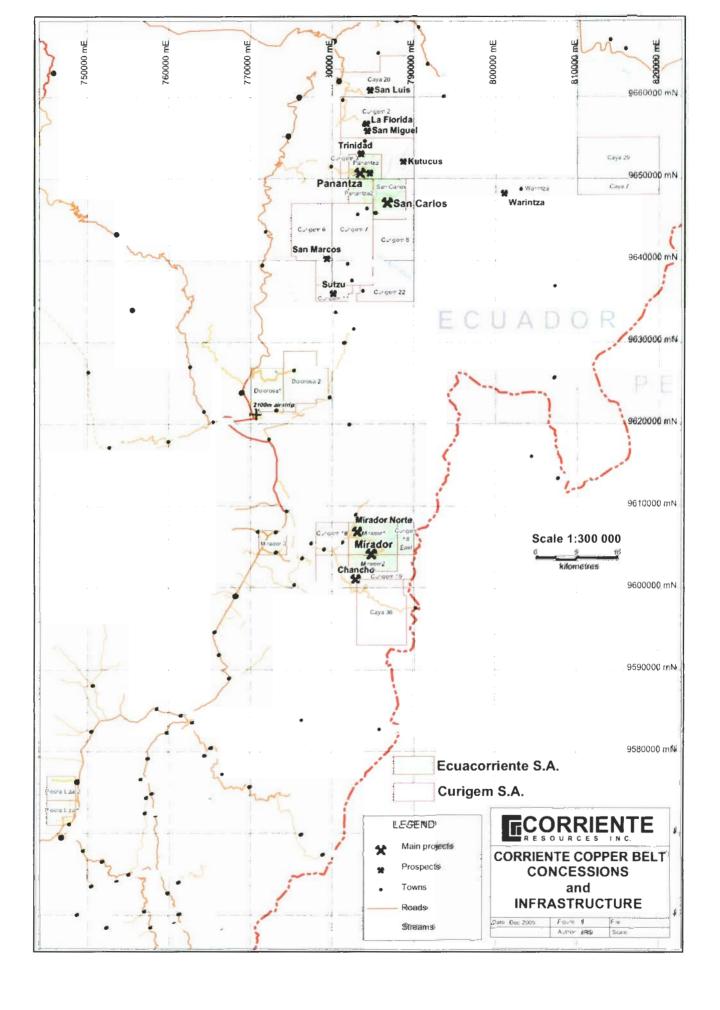
Other than the expiration of the term of the concession registered against the title as described in this paragraph 8, lack of such payment is, according to the Mining Law, the only means by which a concession holder may lose its registration to a property. This letter makes no assessment or contains any opinion regarding issues related to the operation of the concessions. All matters related to the operation of the concessions, such as environmental issues, community relations, filing of environmental and other required reports, completion of environmental plans, among others, have been managed through ECUACORRIENTE S.A. and therefore we cannot give an opinion in such regard.

 According to the Mining Law, concessions registered against title to mining properties have a term of 30 years which can be automatically renewed for further successive 30-year periods, provided that before expiration a written notice of renewal is given by the concession holder.

Please don't hesitate to contact me if you have any additional inquiries.

Sincerely yours,

Dr. Juan Xavier Trejo LAWYER AT LAW



ANNEX A:
ECUACORRIENTE S.A. MINING TITLES

No.	Code	Property name	Concession holder	Title date	Property Register date	Property register county	VALIDITY DATE
7	102211	102211 SAN CARLOS	ECUACORRIENTE	05-feb-03	07-feb-03	SAN JUAN BOSCO	20-jun-32
3	102212	102212 PANANTZA	ECUACORRIENTE	05-feb-03	11-feb-03	LIMON INDANZA	03-jul-32
80	102278	8 102278 PANANTZA 2	ECUACORRIENTE	21-nov-03	03-dic-03	SAN JUAN BOSCO	03-dic-33
7	102502	11 102502 DOLOROSA 1	ECUACORRIENTE	19-ago-05	25-ago-05	GUALAQUIZA	25-ago-35
5	102503	5 102503 DOLOROSA 2	ECUACORRIENTE	11-ago-05	25-ago-05	GUALAQUIZA	25-ago-35
9	500805	6 500805 MIRADOR 2	ECUACORRIENTE	03-feb-03	07-feb-03	PANGUI	23-ago-31
_	500806	CURIGEM 18 Este	500806 CURIGEM 18 Este ECUACORRIENTE	03-feb-03	07-feb-03	PANGUI	23-ago-31
2	500807	2 500807 MIRADOR 1	ECUACORRIENTE	03-feb-03	07-feb-03	PANGUI	23-ago-31
6	500976	9 500976 MIRADOR 3	ECUACORRIENTE	02-may-05	12-may-05	PANGUI	12-may-35
4	500992	4 500992 PIEDRA LIZA 1	ECUACORRIENTE	27-jul-05	10-ago-05	YANTZATZA	10-ago-35
10	500993	10 500993 PIEDRA LIZA 2	ECUACORRIENTE	27-jul-05	10-ago-05	YANTZATZA	10-ago-35

ANNEX A:

CURIGEM S.A. MINING TITLES

No.	. Code	Property name	Concession holder	Title date	Property Register date	Property register county	VALIDITY DATE
1	100074	CURIGEM 2	CURIGEM S.A	06-jun-02	03-jul-02	LIMON INDANZA	03-jul-32
2	4768	CURIGEM 18	CURIGEM S.A	02-ago-01	23-ago-01	PANGUI	23-ago-31
3	4769	CURIGEM 19	CURIGEM S.A	02-ago-01	23-ago-01	PANGUI	23-feb-31
4	100075	CURIGEM 3	CURIGEM S.A	06-jun-02	03-jul-02	SAN JUAN BOSCO	03-jul-32
5	100080	CURIGEM 8	CURIGEM S.A	10-jun-02	20-jun-02	SAN JUAN BOSCO	20-jun-32
9	500200	CAYA 36	CURIGEM S.A	26-jul-01	23-ago-01	PANGUI	23-ago-31
7	101071	CAYA 07	CURIGEM S.A	25-oct-01	16-nov-01	SAN JUAN BOSCO	TEMPORARILY SUSPENDED
8	101074	CAYA 20	CURIGEM S.A	20-sep-01	26-sep-01	LIMON INDANZA	TEMPORARILY SUSPENDED*
6	101160	CAYA 29	CURIGEM S.A	12-sep-01	26-sep-01	SAN JUAN BOSCO	TEMPORARILY SUSPENDED
10	100083	CURIGEM 11	CURIGEM S.A	10-jun-02	20-jun-02	SAN JUAN BOSCO	TEMPORARILY SUSPENDED
1	100128	CURIGEM 22	CURIGEM S.A	10-jun-02	20-jun-02	SAN JUAN BOSCO	TEMPORARILY SUSPENDED
12	100078	CURIGEM 6	CURIGEM S.A	07-jun-02	03-jul-02	SAN JUAN BOSCO	TEMPORARILY SUSPENDED
13	100079	CURIGEM 7	CURIGEM S.A	07-jun-02	03-jul-02	SAN JUAN BOSCO	TEMPORARILY SUSPENDED

Titles are "suspended" until title holder reports there are not access impediments

Appendix B

Mirador Drill Holes M-1 to M-141 Locations, Orientations and Lengths

MO2 784,548.1 9,604,336.8 1,230.6 198.2 90 -90 MO3 785,225.5 9,604,083.8 1,389.8 368.8 360 -90 MO4 784,533.4 9,604,095.9 1,345.2 92.4 90 -90 MO5 784,728.7 9,604,200.7 1,363.9 226.4 90 -90 MO6 784,734.1 9,604,104.1 1,369.3 199.6 90 -90 MO7 784,731.2 9,603,996.8 1,418.7 104.4 90 -90 MO8 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,921.5 9,603,899.3 1,408.0 164 90 -90 M12 784,923.8 9,604,295.8 1,312.6 150.9 90 -90 M12 784,921.1 9,603,788.6 1,459.9 153 90 -90 <th>Hole</th> <th>East</th> <th>North</th> <th>Elev.</th> <th>Depth</th> <th>Azimuth</th> <th>Dip</th>	Hole	East	North	Elev.	Depth	Azimuth	Dip
M03 785,225.5 9,604,083.8 1,389.8 368.8 360 -90 M04 784,533.4 9,604,095.9 1,345.2 92.4 90 -90 M05 784,728.7 9,604,200.7 1,363.9 226.4 90 -90 M06 784,734.1 9,604,104.1 1,369.3 199.6 90 -90 M07 784,831.2 9,603,996.8 1,418.7 104.4 90 -90 M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,921.5 9,603,899.3 1,408.0 164 90 -90 M12 784,923.8 9,604,295.8 1,312.6 150.9 90 -90 M12 784,921.1 9,603,788.6 1,459.9 153 90 -90	M01	784,429.1	9,604,229.0	1,335.9	104.6	180	-70
M04 784,533.4 9,604,095.9 1,345.2 92.4 90 -90 M05 784,728.7 9,604,200.7 1,363.9 226.4 90 -90 M06 784,734.1 9,604,104.1 1,369.3 199.6 90 -90 M07 784,731.2 9,603,996.8 1,418.7 104.4 90 -90 M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,923.8 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,032.8 9,603,887.7 1,386.0 176.2 90 -90 <td>M02</td> <td>784,548.1</td> <td>9,604,336.8</td> <td>1,230.6</td> <td>198.2</td> <td>90</td> <td>-90</td>	M02	784,548.1	9,604,336.8	1,230.6	198.2	90	-90
M05 784,728.7 9,604,200.7 1,363.9 226.4 90 -90 M06 784,734.1 9,604,104.1 1,369.3 199.6 90 -90 M07 784,731.2 9,603,996.8 1,418.7 104.4 90 -90 M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,923.8 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90	M03	785,225.5	9,604,083.8	1,389.8	368.8	360	-90
M06 784,734.1 9,604,104.1 1,369.3 199.6 90 -90 M07 784,731.2 9,603,996.8 1,418.7 104.4 90 -90 M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,874.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90	M04	784,533.4	9,604,095.9	1,345.2	92.4	90	-90
M07 784,731.2 9,603,996.8 1,418.7 104.4 90 -90 M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,877.8 1,386.0 176.2 90 -90 M16 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M17 785,158.2 9,604,299.3 1,298.2 86.3 90 -90	M05	784,728.7	9,604,200.7	1,363.9	226.4	90	-90
M08 784,847.0 9,604,315.5 1,296.3 158.2 90 -90 M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,030.2 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,158.5 9,604,299.3 1,298.2 86.3 90 -90	M06	784,734.1	9,604,104.1	1,369.3	199.6	90	-90
M09 784,837.3 9,604,099.4 1,408.6 150.3 90 -90 M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M20 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M21 785,254.5 9,604,983.8 1,243.9 54.9 90 -90	M07	784,731.2	9,603,996.8	1,418.7	104.4	90	-90
M10 784,821.5 9,603,899.3 1,408.0 164 90 -90 M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,030.2 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,158.2 9,604,299.3 1,298.2 86.3 90 -90 M20 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,983.8 1,243.9 54.9 90 -90	M08	784,847.0	9,604,315.5	1,296.3	158.2	90	-90
M11 784,954.0 9,604,295.8 1,312.6 150.9 90 -90 M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,158.2 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,299.3 1,298.2 86.3 90 -90 M20 785,134.5 9,604,99.3 1,298.2 86.3 90 -90 M20 785,134.5 9,604,98.6 1,319.0 106.1 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90	M09	784,837.3	9,604,099.4	1,408.6	150.3	90	-90
M12 784,923.8 9,604,105.5 1,391.7 211.2 90 -90 M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,299.3 1,298.2 86.3 90 -90 M20 785,134.5 9,604,084.6 1,319.0 106.1 90 -90 M21 785,254.5 9,604,084.6 1,356.4 244.8 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90	M10	784,821.5	9,603,899.3	1,408.0	164	90	-90
M13 784,912.1 9,603,788.6 1,459.9 153 90 -90 M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 <td>M11</td> <td>784,954.0</td> <td>9,604,295.8</td> <td>1,312.6</td> <td>150.9</td> <td>90</td> <td>-90</td>	M11	784,954.0	9,604,295.8	1,312.6	150.9	90	-90
M14 785,031.8 9,604,294.3 1,327.4 150.9 90 -90 M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,229.0 1,335.9 223.4 255 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60<	M12	784,923.8	9,604,105.5	1,391.7	211.2	90	-90
M15 785,030.2 9,603,974.8 1,386.0 176.2 90 -90 M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,280.1 1,335.9 223.4 255 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 </td <td>M13</td> <td>784,912.1</td> <td>9,603,788.6</td> <td>1,459.9</td> <td>153</td> <td>90</td> <td>-90</td>	M13	784,912.1	9,603,788.6	1,459.9	153	90	-90
M16 785,022.8 9,603,887.7 1,385.6 214 90 -90 M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,280.1 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 </td <td>M14</td> <td>785,031.8</td> <td>9,604,294.3</td> <td>1,327.4</td> <td>150.9</td> <td>90</td> <td>-90</td>	M14	785,031.8	9,604,294.3	1,327.4	150.9	90	-90
M17 785,158.2 9,604,410.3 1,304.3 131.1 90 -90 M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,280.1 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -7	M15	785,030.2	9,603,974.8	1,386.0	176.2	90	-90
M18 785,175.5 9,604,299.3 1,298.2 86.3 90 -90 M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M16	785,022.8	9,603,887.7	1,385.6	214	90	-90
M19 785,168.6 9,604,192.6 1,319.0 106.1 90 -90 M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M17	785,158.2	9,604,410.3	1,304.3	131.1	90	-90
M20 785,134.5 9,604,084.6 1,356.4 244.8 90 -90 M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M18	785,175.5	9,604,299.3	1,298.2	86.3	90	-90
M21 785,254.5 9,604,493.8 1,243.9 54.9 90 -90 M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M19	785,168.6	9,604,192.6	1,319.0	106.1	90	-90
M22 784,551.2 9,603,892.8 1,507.7 128 90 -90 M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M20	785,134.5	9,604,084.6	1,356.4	244.8	90	-90
M23 785,342.0 9,604,280.1 1,339.2 400.8 360 -90 M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M21	785,254.5	9,604,493.8	1,243.9	54.9	90	-90
M24 784,515.0 9,604,112.0 1,345.4 69.7 260 -60 M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M22	784,551.2	9,603,892.8	1,507.7	128	90	-90
M25 784,429.1 9,604,229.0 1,335.9 223.4 255 -60 M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M23	785,342.0	9,604,280.1	1,339.2	400.8	360	-90
M26 785,106.6 9,603,790.8 1,464.0 99.2 90 -90 M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M24	784,515.0	9,604,112.0	1,345.4	69.7	260	-60
M27 785,332.8 9,604,204.0 1,370.2 438.9 270 -70 M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M25	784,429.1	9,604,229.0	1,335.9	223.4	255	-60
M28 785,333.9 9,604,093.7 1,325.8 258.5 135 -70	M26	785,106.6	9,603,790.8	1,464.0	99.2	90	-90
	M27	785,332.8	9,604,204.0	1,370.2	438.9	270	-70
M29 785,209.7 9,603,890.7 1,385.1 457.2 360 -90	M28	785,333.9	9,604,093.7	1,325.8	258.5	135	-70
, , , , , , , , , , , , , , , , , , , ,	M29	785,209.7	9,603,890.7	1,385.1	457.2	360	-90
M30 785,124.3 9,603,976.4 1,419.8 175.3 90 -90	M30	785,124.3	9,603,976.4	1,419.8	175.3	90	-90
M31 784,934.0 9,603,982.0 1,360.7 279.5 90 -90	M31	784,934.0	9,603,982.0	1,360.7	279.5	90	-90
M32 785,219.9 9,603,983.5 1,361.2 295.4 90 -90	M32	785,219.9	9,603,983.5	1,361.2	295.4	90	-90

Hole	East	North	Elev.	Depth	Azimuth	Dip
M33	784,932.0	9,604,200.8	1,378.0	285.6	90	-90
M34	785,109.6	9,603,791.7	1,464.0	429.8	115	-70
M35	784,920.8	9,603,890.9	1,414.4	301.8	90	-90
M36	785,121.4	9,603,884.6	1,451.5	175.3	90	-90
M37	785,335.8	9,603,867.2	1,354.1	400	360	-90
M38	785,002.5	9,603,680.1	1,498.1	486.2	360	-90
M39	785,206.5	9,603,683.7	1,410.0	272.5	135	-70
M40	785,205.9	9,603,684.1	1,410.0	298.7	360	-90
M41	785,040.5	9,604,081.1	1,311.8	249.9	90	-90
M42	785,025.3	9,604,190.3	1,330.4	294.1	90	-90
M43	784,903.6	9,603,679.9	1,539.6	399.3	360	-90
M44	784,928.1	9,603,935.7	1,391.9	419.1	360	-90
M45	784,932.9	9,604,038.7	1,364.0	303.3	360	-90
M46	784,822.8	9,604,005.8	1,421.0	408.1	360	-90
M47	784,722.4	9,603,901.2	1,474.6	349	360	-90
M48	784,840.2	9,604,197.6	1,371.3	448.1	360	-90
M49	784,747.3	9,604,313.6	1,356.8	492.3	360	-90
M50	784,551.0	9,604,431.7	1,205.7	341.1	360	-90
M51	784,760.6	9,604,409.4	1,356.1	449.6	360	-90
M52	784,956.3	9,604,395.4	1,290.1	443.5	360	-90
M53	784,734.7	9,604,495.5	1,291.1	198.4	360	-90
M54	784,842.4	9,604,500.8	1,335.5	188.7	360	-90
M55	784,932.3	9,604,490.5	1,316.2	363	360	-90
M56	785,020.6	9,604,511.3	1,240.1	399.9	360	-90
M57	785,015.7	9,604,618.6	1,239.0	250.9	360	-90
M58	785,139.7	9,604,521.8	1,268.0	180.8	360	-90
M59	784,849.1	9,604,420.8	1,355.4	391.7	360	-90
M60	784,667.3	9,604,304.3	1,341.8	410.3	360	-90
M61	784,907.0	9,604,580.2	1,307.0	171.9	360	-90
M62	784,255.9	9,604,470.0	1,310.0	183.3	105	-60
M63	784,705.6	9,604,400.2	1,338.2	400.5	90	-60
M64	784,811.1	9,604,404.5	1,356.8	400.8	110	-60
M65	784,759.4	9,604,359.3	1,362.3	300.2	0	-90

Hole	East	North	Elev.	Depth	Azimuth	Dip
M66	784,844.6	9,604,362.9	1,327.8	300.2	0	-90
M67	784,898.9	9,604,301.3	1,291.1	300.2	0	-90
M68	784,995.2	9,604,298.9	1,313.1	315.5	90	-85
M69	785,098.7	9,604,299.1	1,265.1	269.8	110	-80
M70	785,077.3	9,604,400.1	1,238.2	249.9	0	-90
M71	785,100.1	9,604,197.1	1,284.1	300.2	110	-80
M72	785,157.4	9,604,413.6	1,304.4	286.5	0	-90
M73	785,250.6	9,604,297.5	1,342.5	189	0	-90
M74	785,074.2	9,603,972.5	1,390.4	288	270	-85
M74A	785,074.3	9,603,972.6	1,390.4	73.2	0	-90
M75	784,923.0	9,604,104.2	1,391.8	300.3	135	-60
M76	784,657.3	9,604,004.1	1,442.1	254.5	189	-89
M77	784,841.1	9,604,197.3	1,371.3	300.3	135	-60
M78	784,736.5	9,604,104.8	1,369.0	300.3	90	-55
M79	784,662.6	9,604,110.4	1,409.8	269.8	0	-90
M80	784,749.3	9,604,313.2	1,356.7	300.2	135	-60
M81	784,777.7	9,603,903.2	1,433.0	256	0	-90
M82	784,734.5	9,604,495.6	1,291.1	225.6	90	-65
M83	785,139.4	9,604,608.4	1,222.3	150.9	0	-90
M84	784,553.8	9,604,242.2	1,261.2	249.9	0	-90
M85	784,922.8	9,604,104.8	1,391.4	300.2	225	-60
M86	785,040.9	9,604,080.7	1,311.8	202.7	135	-60
M87	784,633.5	9,604,208.7	1,351.8	300.2	225	-70
M88	784,680.8	9,604,392.1	1,324.0	349.9	315	-80
M89	785,098.7	9,604,300.0	1,265.3	358.1	45	-60
M90	785,224.9	9,604,082.7	1,389.3	298.7	135	-60
M91	784,909.8	9,604,640.0	1,291.2	261.5	0	-90
M92	784,839.5	9,604,567.0	1,291.3	290.2	0	-90
M93	784,639.0	9,604,473.2	1,253.8	249.9	140	-72
M94	784,999.2	9,604,557.5	1,253.4	201.2	0	-90
M95	785,104.2	9,604,467.3	1,258.2	249.9	0	-90
M96	785,165.1	9,604,491.9	1,277.5	249.9	180	-70
M97	785,251.0	9,604,297.4	1,342.4	342.3	105	-75

Hole	East	North	Elev.	Depth	Azimuth	Dip
M98 7	785,215.4	9,604,406.4	1,295.8	251.5	140	-75
M99 7	785,311.6	9,604,346.3	1,291.1	249.9	0	-90
M100 7	785,358.5	9,604,218.9	1,351.1	201.2	0	-90
M101 7	785,259.8	9,604,138.3	1,385.2	278.6	0	-90
M102 7	785,219.5	9,603,983.3	1,361.0	249.9	270	-75
M103 7	785,022.2	9,603,887.5	1,385.4	247.5	90	-65
M104 7	785,017.2	9,603,846.6	1,403.5	209.1	120	-72
M105 7	784,972.2	9,604,184.2	1,362.8	424	135	-80
M106 7	784,976.3	9,604,230.8	1,336.5	417.6	270	-85
M107 7	785,000.3	9,603,763.7	1,458.4	249.9	90	-75
M108 7	785,260.5	9,604,138.2	1,385.1	196.6	135	-70
M109 7	785,092.2	9,603,709.3	1,464.3	177.7	90	-75
M110 7	784,820.8	9,603,709.1	1,534.8	230.1	90	-77
M111 7	784,813.1	9,603,784.8	1,462.3	179.5	135	-70
M112 7	784,699.5	9,603,858.2	1,475.1	231.3	135	-70
M113 7	784,652.3	9,603,906.3	1,482.3	250.2	0	-90
M114 7	784,614.8	9,603,950.1	1,461.8	242.3	270	-80
M115 7	784,610.7	9,604,022.8	1,413.4	201.2	220	-85
M116 7	784,694.0	9,604,262.4	1,362.1	431.3	310	-75
M117 7	784,589.4	9,604,122.1	1,354.8	135.7	160	-72
M118 7	784,394.8	9,604,279.3	1,327.8	150.9	0	-90
M119 7	784,482.8	9,604,293.3	1,271.4	170.7	0	-90
M120 7	784,839.2	9,604,567.7	1,291.4	161.2	335	-70
M121 7	785,139.3	9,604,521.7	1,267.7	254.8	260	-70
M122 7	784,901.9	9,604,542.2	1,319.1	249.9	0	-90
M123 7	784,801.9	9,604,503.1	1,306.7	225.6	90	-65
M124 7	784,735.2	9,604,494.9	1,291.2	231	135	-65
M125 7	784,959.9	9,604,459.9	1,306.0	286.5	90	-70
M126 7	784,878.9	9,604,460.2	1,343.8	285	90	-70
M127 7	784,674.9	9,604,361.2	1,332.7	251.5	90	-70
M128 7	784,616.1	9,604,405.6	1,255.4	100.9	0	-90
M129 7	784,599.4	9,604,342.5	1,267.7	216.7	135	-80
M130 7	784,568.0	9,604,288.6	1,264.9	120.4	0	-90

Hole	East	North	Elev.	Depth	Azimuth	Dip
M131	784,553.6	9,604,242.3	1,260.9	225.9	270	-70
M132	784,545.6	9,604,203.5	1,262.3	151.2	180	-75
M133	784,554.2	9,604,242.4	1,261.0	201.5	110	-60
M134	784,462.1	9,604,171.0	1,337.9	151.2	0	-90
M135	784,671.3	9,604,206.8	1,377.1	360.9	0	-90
M136	784,743.1	9,604,159.2	1,360.0	195.4	90	-80
M137	784,673.1	9,604,156.5	1,400.7	151.2	0	-90
M138	784,741.4	9,604,065.4	1,378.9	250.2	90	-80
M139	785,051.8	9,604,267.2	1,321.6	94.8	135	-70
M139A	785,051.8	9,604,267.2	1,321.6	96.3	135	-70
M140	784,847.7	9,604,288.5	1,297.4	250.2	135	-70
M141	785,020.4	9,604,407.7	1,257.6	201.2	140	-70

Appendix C

Sample Descriptive Statistics For Copper, Gold, and Silver

Zones	Material	1000	Grade	100,200,300	Lithology	10,20		
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	6,556	0.600	0.600	0.238	0.40	0.01	1.87	%
ppb Au MDA	6,556	178.000	201.024	124.445	0.62	0.0	3159	ppb
Zones	Material	1000	Grade	0,100,200	Lithology	10,20		
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	2,570	0.330	0.353	0.192	0.54	0.01	1.87	%
ppb Au MDA	2,570	116.000	130.913	90.289	0.69	0.0	1079	ppb
Zones	Material	>=1000	Grade	100,200,300	Lithology	10,20		
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	7,631	0.580	0.562	0.315	0.56	0.01	3.52	%
ppb Au MDA	7,631	181.000	205.398	126.263	0.61	0.0	3159	ppb
Zones	Material	>=1000	Grade	0,100,200	Lithology	10,20		
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	2,957	0.320	0.339	0.219	0.65	0.01	2.24	%
ppb Au MDA	2,957	116.000	133.145	93.606	0.70	0.0	1486	ppb
			· · ·					
Zones	Material	1000	Grade	NA	Lithology	30 E	Early dikes	
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	1,196	0.400	0.423	0.223	0.53	0.01	1.65	%
ppb Au MDA	1,196	126.500	150.301	125.547	0.84	3.0	2230	ppb
Zones	Material	all X000s	Grade	NA	Lithology		Early dikes	
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	1,361	0.400	0.423	0.223	0.53	0.01	1.74	%
ppb Au MDA	1,361	126.500	150.301	125.547	0.84	3.0	2230	ppb
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Zones	Material	1000	Grade	NA	Lithology		Post-mineral bre	
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	654	0.020	0.062	0.144	2.33	0.00	2.27	%
ppb Au MDA	654	15.000	38.055	117.516	3.09	0.0	2428	ppb
_								
Zones	Material	all X000s	Grade	NA	Lithology		Early dikes	
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	688	0.010	0.060	0.140	2.34	0.00	2.27	%
ppb Au MDA	688	10.000	37.845	115.286	3.05	0.0	2428	ppb
7								
Zones	Material	1000	Grade	NA NA	Lithology		Post-mineral dik	
0/ O NADA	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	732	0.121	0.197	0.216	1.09	0.00	1.15	%
ppb Au MDA	732	40.500	75.034	96.222	1.28	0.0	868	ppb
Zones	Mata-!-!	all V000-	Crada	NIA	Lithology	E0 '	ata Dikas	
Zones	Material	all X000s	Grade	NA Std Dov	Lithology		_ate Dikes	He:4-
% Cu MDA	Valid N 780	Median	Mean 0.187	Std.Dev. 0.210	CV 1.12	Minimum	Maximum	Units
ppb Au MDA	780 780	0.090 31.000	74.523	95.825	1.12	0.00 0.0	1.15 868	% ppb
Pho Va MDV	700	31.000	14.023	33.023	1.23	0.0	000	μμυ
Zones	Material	2000	Grade	NA	Lithology	NA S	Supergene/enric	had
_01163	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	
% Cu MDA	483	0.960	1.015	0.585	0.58	0.07	3.52	Units %
ppb Au MDA	483	200.000	223.763	176.462	0.38	9.0	2838	ppb
1. L	100	_00.000		110.402	0.70	0.0		PP2
Zones	Material	3000	Grade	NA	Lithology	NA I	Mixed	
_000	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA	282	0.290	0.336	0.319	0.95	0.00	2.3	%
ppb Au MDA	282	137.000	160.090	109.240	0.68	4.0	825	ppb
Ebo va MDV	202	.07.000	.00.000	100.240	0.00	т.0	020	440
_								
Zones	Material	4 000	Grade	NΔ	Lithology	NA I	eached	
Zones	Material Valid N	4000 Median	Grade	NA Std Dev	Lithology		_eached	Unite
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
% Cu MDA ppb Au MDA								Units % ppb

		Zo	one	30				
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
Ag ppm	1,143	1.000	1.520	2.660	1.75	0.000	50.00	ppm
		Zo	ne	40				
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
Ag ppm	454	0.200	0.320	0.500	1.56	0.000	5.00	ppm
		Zo	ne	50				
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
Ag ppm	516	0.400	1.030	3.310	3.21	0.000	50.00	ppm
		Zo	ne	12340				
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
Ag ppm	1,923	0.900	1.000	1.100	1.10	0.000	20.00	ppm
		Zo	ne	12342				
	Valid N	Median	Mean	Std.Dev.	CV	Minimum	Maximum	Units
Aa ppm	5.175	1.300	1.630	1.620	0.99	0.000	40.10	mag